

Quality by Design for ANDAs: An Example for Immediate-Release Dosage Forms

Introduction to the Example

This is an example pharmaceutical development report illustrating how ANDA applicants can move toward implementation of Quality by Design (QbD). The purpose of the example is to illustrate the types of pharmaceutical development studies ANDA applicants may use as they implement QbD in their generic product development and to promote discussion on how OGD would use this information in review.

Although we have tried to make this example as realistic as possible, the development of a real product may differ from this example. The example is for illustrative purposes and, depending on applicants' experience and knowledge, the degree of experimentation for a particular product may vary. The impact of experience and knowledge should be thoroughly explained in the submission. The risk assessment process is one avenue for this explanation. At many places in this example, alternative pharmaceutical development approaches would also be appropriate.

Notes to the reader are included in italics throughout the text. Questions and comments may be sent to GenericDrugs@fda.hhs.gov

Pharmaceutical Development Report Example QbD for IR Generic Drugs

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1.1 Executive Summary

The following pharmaceutical development report summarizes the development of Generic Acetripitan Tablets, 20 mg, a generic version of the reference listed drug (RLD), Brand Acetripitan Tablets, 20 mg. The RLD is an immediate release (IR) tablet indicated for the relief of moderate to severe physiological symptoms. We used Quality by Design (QbD) to develop generic acetripitan IR tablets that are therapeutically equivalent to the RLD.

Initially, the quality target product profile (QTPP) was defined based on the properties of the drug substance, characterization of the RLD product, and consideration of the RLD label and intended patient population. Identification of critical quality attributes (CQAs) was based on the severity of harm to a patient (safety and efficacy) resulting from failure to meet that quality attribute of the drug product. Our investigation during pharmaceutical development focused on those CQAs that could be impacted by a realistic change to the drug product formulation or manufacturing process. For generic acetripitan tablets, these CQAs included assay, content uniformity, dissolution and degradation products.

Acetripitan is a poorly soluble, highly permeable Biopharmaceutics Classification System (BCS) Class II compound. As such, initial efforts focused on developing a dissolution method that would be able to predict in vivo performance. The developed in-house dissolution method uses 900 mL of 0.1 N HCl with 1.0% w/v sodium lauryl sulfate (SLS) in USP apparatus 2 stirred at 75 rpm. This method is capable of differentiating between formulations manufactured using different acetripitan particle size distributions (PSD) and predicting their in vivo performance in the pilot bioequivalence (BE) study.

Risk assessment was used throughout development to identify potentially high risk formulation and process variables and to determine which studies were necessary to achieve product and process understanding in order to develop a control strategy. Each risk assessment was then updated after development to capture the reduced level of risk based on our improved product and process understanding.

For formulation development, an in silico simulation was conducted to evaluate the potential effect of acetripitan PSD on in vivo performance and a d_{90} of 30 μm or less was selected. Roller compaction (RC) was selected as the granulation method due to the potential for thermal degradation of acetripitan during the drying step of a wet granulation process. The same types of excipients as the RLD product were chosen. Excipient grade selection was based on experience with previously approved ANDA 123456 and ANDA 456123 which both used roller compaction. Initial excipient binary mixture compatibility studies identified a potential interaction between acetripitan and magnesium stearate. However, at levels representative of the final formulation, the interaction was found to be negligible. Furthermore, the potential interaction between acetripitan and magnesium stearate is limited by only including extragranular magnesium stearate.

Two formulation development design of experiments (DOE) were conducted. The first DOE investigated the impact of acetripitan PSD and levels of intragranular lactose, microcrystalline cellulose and croscarmellose sodium on drug product CQAs. The second DOE studied the levels

of extragranular talc and magnesium stearate on drug product CQAs. The formulation composition was finalized based on the knowledge gained from these two DOE studies.

An in-line near infrared (NIR) spectrophotometric method was validated and implemented to monitor blend uniformity and to reduce the risk associated with the pre-roller compaction blending and lubrication step. Roller pressure, roller gap and mill screen orifice size were identified as critical process parameters (CPPs) for the roller compaction and integrated milling process step and acceptable ranges were identified through the DOE. Within the ranges studied during development of the final blending and lubrication step, magnesium stearate specific surface area (5.8-10.4 m²/g) and number of revolutions (60-100) did not impact the final product CQAs. During tablet compression, an acceptable range for compression force was identified and force adjustments should be made to accommodate the ribbon relative density (0.68-0.81) variations between batches in order to achieve optimal hardness and dissolution.

Scale-up principles and plans were discussed for scaling up from lab (5.0 kg) to pilot scale (50.0 kg) and then proposed for commercial scale (150.0 kg). A 50.0 kg cGMP exhibit batch was manufactured at pilot scale and demonstrated bioequivalence in the pivotal BE study. The operating ranges for identified CPPs at commercial scale were proposed and will be qualified and continually verified during routine commercial manufacture.

Finally, we proposed a control strategy that includes the material attributes and process parameters identified as potentially high risk variables during the initial risk assessments. Our control strategy also includes in-process controls and finished product specifications. The process will be monitored during the lifecycle of the product and additional knowledge gained will be utilized to make adjustments to the control strategy as appropriate.

The development time line for Generic Acetripitan Tablets, 20 mg, is presented in Table 1.

Table 1. Development of Generic Acetripitan Tablets, 20 mg, presented in chronological order

Study	Scale	Page
Analysis of the Reference Listed Drug product	N/A	6
Evaluation of the drug substance properties	N/A	18
Excipient compatibility	N/A	25
In silico simulation to select acetripitan PSD for product development	N/A	30
Attempted direct compression of RLD formulation	Lab (1.0 kg)	32
Lab scale roller compaction process feasibility study	Lab (1.0 kg)	65
Formulation Development Study #1: Effect of acetripitan PSD, MCC/Lactose ratio and CCS level	Lab (1.0 kg)	33
Dissolution testing using FDA-recommended method	N/A	36
In-house dissolution method development	N/A	13
Formulation Development Study #2: Effect of extragranular magnesium stearate and talc level	Lab (1.0 kg)	44
Formulations with different acetripitan PSD for pilot BE study	Lab (1.0 kg)	14
Dissolution testing of formulations for pilot BE study	N/A	16
Pilot BE Study #1001	N/A	14
Pre-roller compaction blending and lubrication process development: effect of acetripitan PSD and number of revolutions	Lab (5.0 kg)	56
Development of in-line NIR method for blending endpoint determination	Lab (5.0 kg)	59
Roller compaction and integrated milling process development: effect of roller pressure, roller gap, mill speed and mill screen orifice size	Lab (5.0 kg)	65
Final blending and lubrication process development: effect of magnesium stearate specific surface area and number of revolutions	Lab (5.0 kg)	79
Tablet compression process development: effect of main compression force, press speed, and ribbon relative density	Lab (5.0 kg)	83
Scale-up strategy from lab to pilot and commercial scale	N/A	90
Exhibit batch for pivotal BE study	Pilot (50.0 kg)	95

1.2 Analysis of the Reference Listed Drug Product

1.2.1 Clinical

The Reference Listed Drug (RLD) is Brand Acetripitan Tablets, 20 mg, and was approved in the United States in 2000 (NDA 211168) for therapeutic relief of moderate to severe symptoms. The RLD is an unscored immediate release (IR) tablet with no cosmetic coating. The tablet needs to be swallowed “as is” without any intervention. Thus, the proposed generic product will also be an unscored IR tablet with no cosmetic coating. The maximum daily dose in the label is 40 mg (i.e., one tablet twice per day). A single tablet is taken per dose with or without food. Brand Acetripitan Tablets, 20 mg, should be swallowed whole with a glass of water.

1.2.2 Pharmacokinetics

Acetripitan is well absorbed after oral administration. The median T_{max} is 2.5 hours (h) in patients. The mean absolute bioavailability of acetripitan is approximately 40%. The AUC and C_{max} of acetripitan are increased by approximately 8% to 12% following oral dosing with a high fat meal. The terminal elimination half-life of acetripitan is approximately 4 hours.

1.2.3 Drug Release

Drug release is usually the rate limiting process for absorption of a Biopharmaceutics Classification System (BCS) Class II compound like acetripitan due to its low solubility. Therefore, the dissolution of the RLD tablets was thoroughly evaluated. Initially, the dissolution method recommended in the FDA dissolution methods database for this product was utilized (900 mL of 0.1 N HCl with 2.0% w/v sodium lauryl sulfate (SLS) using USP apparatus 2 (paddle) at 75 rpm). The temperature of the dissolution medium was maintained at 37 ± 0.5 °C and the drug concentration was determined using UV spectroscopy at a wavelength of 282 nm. The drug release of RLD tablets was also obtained at different medium pH (pH 4.5 acetate buffer and pH 6.8 phosphate buffer) with 2.0% w/v SLS. As shown in Figure 1, RLD tablets exhibited a very rapid dissolution using the FDA-recommended method without any sensitivity to medium pH.

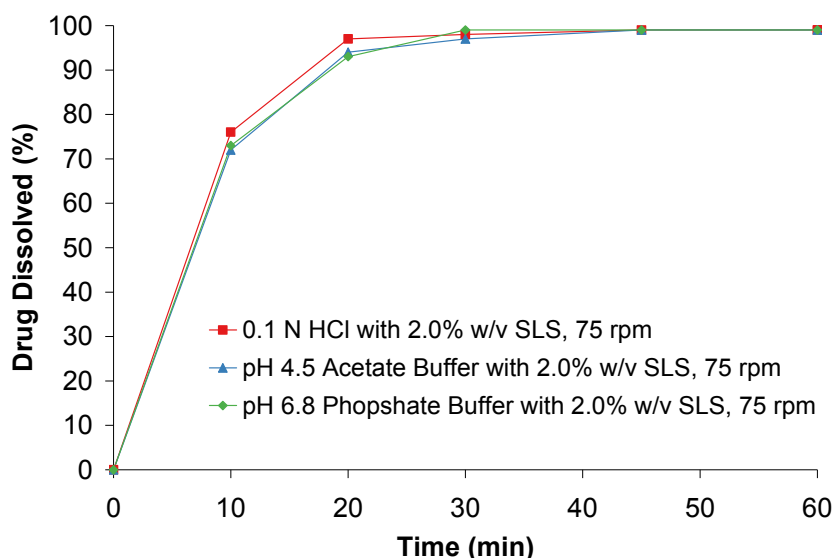


Figure 1. RLD dissolution profile in 900 mL of medium (pH as shown) with 2.0% w/v SLS using USP apparatus 2 at 75 rpm

1.2.4 Physicochemical Characterization

The physicochemical characterization of the RLD tablet is summarized in Table 2. Characterization included determination of the level of ACE12345, a known degradant, in near expiry product.

Table 2. Physicochemical characterization of Brand Acetripitan Tablets, 20 mg

Description	White round tablet debossed with ACE
Batch No.	A6970R
Expiry date	November 2011
Strength (mg)	20
Average weight (mg)	201.2
Score	No
Coating	Uncoated
Diameter (mm)	8.02-8.05
Thickness (mm)	2.95-3.08
Volume (mm³)	150.02 average measured using image analysis
Hardness (kP)	7.4-10.1
Disintegration time (min)	1.4-1.6
Disintegration observation	Rapidly disintegrates into fine powder
Assay (% w/w of label claim)	99.7-100.2
Related Compound 1 (RC1) (%)	ND
Related Compound 2 (RC2) identified as ACE12345 (%)	0.41-0.44
Related Compound 3 (RC3) (%)	ND
Related Compound 4 (RC4) (%)	ND
Highest individual unknown (%)	0.07-0.09

1.2.5 Composition

Based on the RLD labeling, patent literature and reverse engineering, Table 3 lists the composition of Brand Acetripitan Tablets, 20 mg. The level provided for each excipient is consistent with previous experience and is below the level listed in the inactive ingredient database (IID) for FDA-approved oral solid dosage forms.

Table 3. Composition of Brand Acetripitan Tablets, 20 mg

Component	Function	Unit (mg per tablet)	Unit (% w/w)
Acetripitan, USP	Active	20.0	10
Lactose Monohydrate, NF	Filler	64-86	32-43
Microcrystalline Cellulose (MCC), NF	Filler	72-92	36-46
Croscarmellose Sodium (CCS), NF	Disintegrant	2-10	1-5
Magnesium Stearate, NF*	Lubricant	2-6	1-3
Talc, NF	Glidant/Lubricant	1-10	0.5-5
Total tablet weight		200	100

*Magnesium stearate level estimated by EDTA titration of magnesium.

1.3 Quality Target Product Profile for the ANDA Product

Note to Reader: The quality target product profile (QTPP) is “a prospective summary of the quality characteristics of a drug product that ideally will be achieved to ensure the desired quality, taking into account safety and efficacy of the drug product.”¹ The QTPP is an essential element of a QbD approach and forms the basis of design of the generic product. For ANDAs, the target should be defined early in development based on the properties of the drug substance (DS), characterization of the RLD product and consideration of the RLD label and intended patient population. The QTPP includes all product attributes that are needed to ensure equivalent safety and efficacy to the RLD. This example is for a simple IR tablet; other products would include additional attributes in the QTPP. By beginning with the end in mind, the result of development is a robust formulation and manufacturing process with a control strategy that ensures the performance of the drug product.

A critical quality attribute (CQA) is “a physical, chemical, biological, or microbiological property or characteristic that should be within an appropriate limit, range, or distribution to ensure the desired product quality.”¹ The identification of a CQA from the QTPP is based on the severity of harm to a patient should the product fall outside the acceptable range for that attribute.

All quality attributes are target elements of the drug product and should be achieved through a good quality management system as well as appropriate formulation and process design and development. From the perspective of pharmaceutical development, we only investigate the subset of CQAs of the drug product that also have a high potential to be impacted by the formulation and/or process variables. Our investigation culminates in an appropriate control strategy.



Based on the clinical and pharmacokinetic (PK) characteristics as well as the in vitro dissolution and physicochemical characteristics of the RLD, a quality target product profile (QTPP) was defined for Generic Acetripitan Tablets, 20 mg (see Table 4).

¹ ICH Harmonised Tripartite Guideline: Q8(R2) Pharmaceutical Development. August 2009.

Table 4. Quality Target Product Profile (QTPP) for Generic Acetripitan Tablets, 20 mg

QTPP Elements		Target	Justification
Dosage form		Tablet	Pharmaceutical equivalence requirement: same dosage form
Dosage design		Immediate release tablet without a score or coating	Immediate release design needed to meet label claims
Route of administration		Oral	Pharmaceutical equivalence requirement: same route of administration
Dosage strength		20 mg	Pharmaceutical equivalence requirement: same strength
Pharmacokinetics		Immediate release enabling T_{max} in 2.5 hours or less; Bioequivalent to RLD	Bioequivalence requirement Needed to ensure rapid onset and efficacy
Stability		At least 24-month shelf-life at room temperature	Equivalent to or better than RLD shelf-life
Drug product quality attributes	Physical Attributes	Pharmaceutical equivalence requirement: Must meet the same compendial or other applicable (quality) standards (i.e., identity, assay, purity, and quality).	
	Identification		
	Assay		
	Content Uniformity		
	Dissolution		
	Degradation Products		
	Residual Solvents		
	Water Content		
Microbial Limits			
Container closure system		Container closure system qualified as suitable for this drug product	Needed to achieve the target shelf-life and to ensure tablet integrity during shipping
Administration/Concurrence with labeling		Similar food effect as RLD	RLD labeling indicates that a high fat meal increases the AUC and C_{max} by 8-12%. The product can be taken without regard to food.
Alternative methods of administration		None	None are listed in the RLD label.

Table 5 summarizes the quality attributes of generic acetripitan tablets and indicates which attributes were classified as drug product critical quality attributes (CQAs). For this product, assay, content uniformity (CU), dissolution and degradation products are identified as the subset of CQAs that have the potential to be impacted by the formulation and/or process variables and, therefore, will be investigated and discussed in detail in subsequent formulation and process development studies.

On the other hand, CQAs including identity, residual solvents and microbial limits which are unlikely to be impacted by formulation and/or process variables will not be discussed in detail in the pharmaceutical development report. However, these CQAs are still target elements of the QTPP and are ensured through a good pharmaceutical quality system and the control strategy.

Table 5. Critical Quality Attributes (CQAs) of Generic Acetripitan Tablets, 20 mg

Quality Attributes of the Drug Product		Target	Is this a CQA?	Justification
Physical Attributes	Appearance	Color and shape acceptable to the patient. No visual tablet defects observed.	No	Color, shape and appearance are not directly linked to safety and efficacy. Therefore, they are not critical. The target is set to ensure patient acceptability.
	Odor	No unpleasant odor	No	In general, a noticeable odor is not directly linked to safety and efficacy, but odor can affect patient acceptability. For this product, neither the drug substance nor the excipients have an unpleasant odor. No organic solvents will be used in the drug product manufacturing process.
	Size	Similar to RLD	No	For comparable ease of swallowing as well as patient acceptance and compliance with treatment regimens, the target for tablet dimensions is set similar to the RLD.
	Score configuration	Unscored	No	The RLD is an unscored tablet; therefore, the generic tablet will be unscored. Score configuration is not critical for the acetripitan tablet.
	Friability	NMT 1.0% w/w	No	Friability is a routine test per compendial requirements for tablets. A target of NMT 1.0% w/w of mean weight loss assures a low impact on patient safety and efficacy and minimizes customer complaints.
Identification		Positive for acetripitan	Yes*	Though identification is critical for safety and efficacy, this CQA can be effectively controlled by the quality management system and will be monitored at drug product release. Formulation and process variables do not impact identity. Therefore, this CQA will not be discussed during formulation and process development.
Assay		100% w/w of label claim	Yes	Assay variability will affect safety and efficacy. Process variables may affect the assay of the drug product. Thus, assay will be evaluated throughout product and process development.
Content Uniformity (CU)		Conforms to USP <905> Uniformity of Dosage Units	Yes	Variability in content uniformity will affect safety and efficacy. Both formulation and process variables impact content uniformity, so this CQA will be evaluated throughout product and process development.
Dissolution		NLT 80% at 30 minutes in 900 mL of 0.1 N HCl with 1.0% w/v SLS using USP apparatus 2 at 75 rpm	Yes	Failure to meet the dissolution specification can impact bioavailability. Both formulation and process variables affect the dissolution profile. This CQA will be investigated throughout formulation and process development.

Example QbD IR Tablet Module 3 Quality 3.2.P.2 Pharmaceutical Development

of the Drug Product	Target	Is this a CQA?	Justification
Degradation Products	ACE12345: NMT 0.5%, Any unknown impurity: NMT 0.2%, Total impurities: NMT 1.0%	Yes	Degradation products can impact safety and must be controlled based on compendial/ICH requirements or RLD characterization to limit patient exposure. ACE12345 is a common degradant of acetriptan and its target is based on the level found in near expiry RLD product. The limit for total impurities is also based on RLD analysis. The target for any unknown impurity is set according to the ICH identification threshold for this drug product. Formulation and process variables can impact degradation products. Therefore, degradation products will be assessed during product and process development.
Residual Solvents	USP <467> option 1	Yes*	Residual solvents can impact safety. However, no solvent is used in the drug product manufacturing process and the drug product complies with USP <467> Option 1. Therefore, formulation and process variables are unlikely to impact this CQA.
Water Content	NMT 4.0% w/w	No	Generally, water content may affect degradation and microbial growth of the drug product and can be a potential CQA. However, in this case, acetriptan is not sensitive to hydrolysis and moisture will not impact stability.
Microbial Limits	Meets relevant pharmacopoeia criteria	Yes*	Non-compliance with microbial limits will impact patient safety. However, in this case, the risk of microbial growth is very low because roller compaction (dry granulation) is utilized for this product. Therefore, this CQA will not be discussed in detail during formulation and process development.

*Formulation and process variables are unlikely to impact the CQA. Therefore, the CQA will not be investigated and discussed in detail in subsequent risk assessment and pharmaceutical development. However, the CQA remains a target element of the drug product profile and should be addressed accordingly.

1.4 Dissolution Method Development and Pilot Bioequivalence Studies

Note to Reader: A pharmaceutical development report should document the selection of the dissolution method used in pharmaceutical development. This method (or methods) may differ from the FDA-recommended dissolution method and the quality control method used for release testing.

1.4.1 Dissolution Method Development

Acetripitan is a BCS Class II compound displaying poor aqueous solubility (less than 0.015 mg/mL) across the physiological pH range. As such, development of a dissolution method that can act as the best available predictor of equivalent pharmacokinetics to the RLD was pursued to allow assessment of acetripitan tablets manufactured during development.

The target is an immediate release product, so dissolution in the stomach and absorption in the upper small intestine is expected suggesting the use of dissolution medium with low pH. Development began with the quality control dissolution method recommended for this product by the FDA: 900 mL of 0.1 N HCl with 2.0% w/v SLS using USP apparatus 2 at 75 rpm. Initial development formulations (Batches 1-11) exhibited rapid dissolution (NLT 90% dissolved in 30 minutes (min)) and were comparable to the RLD. It became a challenge for the team to select the formulations which might perform similarly to the RLD in vivo. The solubility of acetripitan in various media was determined (Table 6) and suggests that the solubility of acetripitan in 0.1 N HCl with 1.0% w/v SLS is similar to its solubility in biorelevant media.

Table 6. Acetripitan solubility in different media

Media	Solubility
--	(mg/mL)
Biorelevant FaSSGF ²	0.12
Biorelevant FaSSIF-V2 ²	0.18
0.1 N HCl with 0.5% SLS	0.075
0.1 N HCl with 1.0% SLS	0.15
0.1 N HCl with 2.0% SLS	0.3

Figure 2 presents the dissolution of the RLD in 0.1 N HCl with different SLS concentrations.

² Jantratid E, Janssen N, Reppas C, and Dressman JB. Dissolution Media Simulating Conditions in the Proximal Human Gastrointestinal Tract: An Update. Pharm Res 25:1663-1676, 2008.

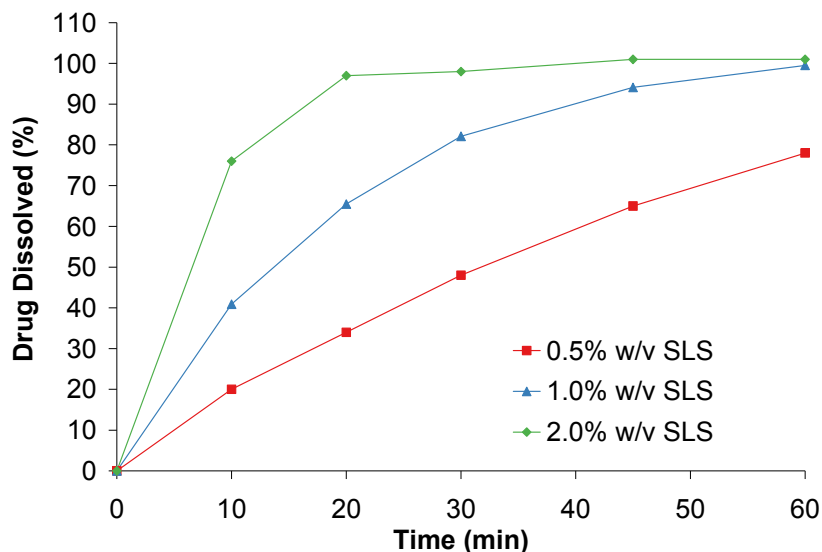


Figure 2. RLD dissolution profile in 900 mL of 0.1 N HCl with various SLS concentrations using USP apparatus 2 at 75 rpm

The dissolution method selected for product development uses 900 mL of 0.1 N HCl with 1.0% w/v SLS in a dissolution apparatus equipped with paddles (speed 75 rpm) and maintained at a temperature of 37°C, followed by UV spectroscopy at a wavelength of 282 nm. Dissolution in 1.0% w/v SLS is not sensitive to medium pH (similar in 0.1 N HCl, pH 4.5 buffer and pH 6.8 buffer) (*data not shown*). Additionally, this method is capable of detecting dissolution changes in the drug product caused by deliberately varying the drug substance (DS) particle size distribution (PSD) (*see Section 1.4.2*).

1.4.2 Pilot Bioequivalence Study

Note to Reader: For low solubility drugs, pilot bioequivalence (BE) studies are invaluable to demonstrate that the in vitro dissolution used is appropriate. When pilot bioequivalence studies are conducted, the following is an example of how they should be described in the development report to support controls on critical attributes such as particle size and to understand the relationship between in vitro dissolution and in vivo performance. Inclusion of formulations that perform differently will help to determine if there is a useful in vivo in vitro relationship.

The formulation development studies identified drug substance particle size distribution as the most significant factor that impacts drug product dissolution (*see Section 2.2.1.4*). In order to understand the potential clinical relevance of drug substance particle size distribution on in vivo performance, a pilot bioequivalence (BE) study (Study # 1001) was performed in 6 healthy subjects (four-way crossover: three prototypes and the RLD at a dose of 20 mg).

The formulation used to produce the three prototypes and the composition is shown in Table 7. The only difference between each prototype was the drug substance particle size distribution. Drug substance Lot #2, #3 and #4 with a d_{90} of 20 μm , 30 μm and 45 μm was used for prototype

Batch 18, 19, and 20, respectively. Characterization of the drug substance lots is provided in Section 2.2.1.2, Table 19.

Table 7. Formulation of Generic Acetripitan Tablets, 20 mg, used in Pilot BE Study #1001

Ingredient	Function	Composition	
		(mg per tablet)	(% w/w)
Acetripitan	Active	20.0	10.0
Intragranular Excipients			
Lactose Monohydrate, NF	Filler	79.0	39.5
Microcrystalline Cellulose (MCC), NF	Filler	79.0	39.5
Croscarmellose Sodium (CCS), NF	Disintegrant	10.0	5.0
Talc, NF	Glidant/lubricant	5.0	2.5
Extragranular Excipients			
Magnesium Stearate, NF	Lubricant	1.2	0.6
Talc, NF	Glidant/lubricant	5.8	2.9
Total Weight		200.0	100

The pharmacokinetic results are presented in Figure 3 and Table 8.

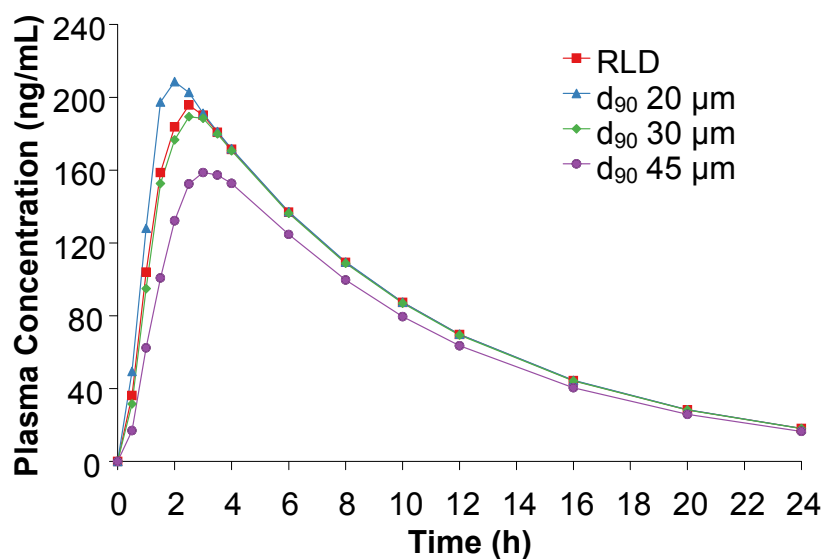


Figure 3. Mean PK profiles obtained from Pilot BE Study #1001

Table 8. Pharmacokinetic parameters (geometric mean) from Pilot BE Study #1001

Pharmacokinetic Parameters	Lot #2 (d ₉₀ 20 µm)	Lot #3 (d ₉₀ 30 µm)	Lot #4 (d ₉₀ 45 µm)	N/A (RLD)
Drug Product Batch No.	18	19	20	A6971R
AUC _∞ (ng/ml h)	2154.0	2070.7	1814.6	2095.3
AUC _{0-t} (ng/ml h)	1992.8	1910.6	1668.0	1934.5
C _{max} (ng/ml)	208.55	191.07	158.69	195.89
T _{max} (h)	2.0	2.5	3.0	2.5
t _{1/2} (h)	6.0	6.0	6.0	6.0
Test/Reference AUC _∞ Ratio	1.028	0.988	0.866	--
Test/Reference AUC _{0-t} Ratio	1.030	0.988	0.862	--
Test/Reference C _{max} Ratio	1.065	0.975	0.810	--

According to the literature³, when the mean C_{max} and AUC responses of 2 drug products differ by more than 12-13%, they are unlikely to meet the bioequivalence limits of 80-125%. Therefore, the predefined selection criterion was a mean particle size that yielded both a C_{max} ratio and an AUC ratio for test to reference between 0.9 and 1.11. The results of the PK study indicated that a drug substance particle size distribution with a d₉₀ of 30 µm or less showed similar in vivo performance based on test to reference ratio calculations for AUC and C_{max}. A drug substance particle size distribution with a d₉₀ of 45 µm did not meet the predefined criterion of a test to reference ratio for C_{max} and AUC between 0.9 and 1.11. The results confirmed the in silico simulation data obtained during preformulation work (*see Section 2.2.1.2*).

In order to understand the relationship between in vitro dissolution and in vivo performance, the dissolution test was performed on the three prototypes and the RLD using the in-house versus the FDA-recommended dissolution method. The results are presented in Figure 4 and Figure 5, respectively. The data indicated that the in-house dissolution method (with 1.0% w/v SLS) is capable of differentiating formulations manufactured using different drug substance particle size distributions. However, the FDA-recommended dissolution method (with 2.0% w/v SLS) is not sensitive to deliberate formulation changes in the drug substance particle size distribution for this BCS class II compound.

³ B.M. Davit, et al. Comparing generic and innovator drugs: a review of 12 years of bioequivalence data from the United States Food and Drug Administration. *The Annals of Pharmacotherapy*, 2009, 43: 1583-1597.

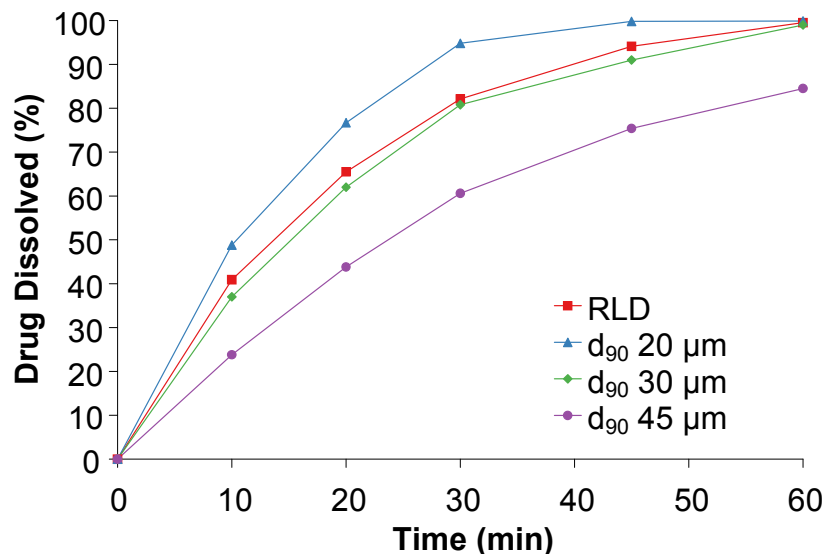


Figure 4. Dissolution of acetriptan tablets (RLD and three prototypes) using in-house method (900 mL of 0.1 N HCl with 1.0% w/v SLS using USP apparatus 2 at 75 rpm)

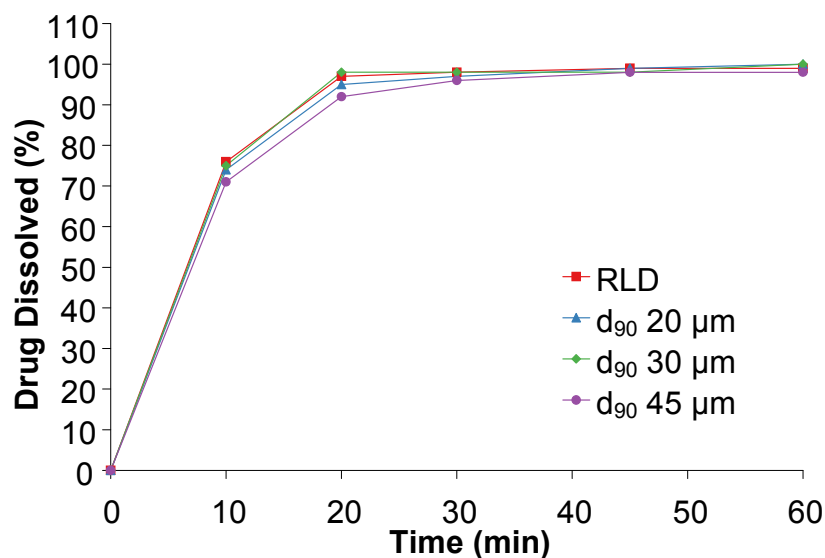


Figure 5. Dissolution of acetriptan tablets (RLD and three prototypes) using FDA-recommended method (900 mL of 0.1 N HCl with 2.0% w/v SLS using USP apparatus 2 at 75 rpm)

The AUC_{0-t} ratio and C_{max} ratio between the prototypes and the RLD were plotted versus the percentage of drug dissolved using both the in-house and FDA-recommended dissolution methods. The results are presented in Figure 6 and suggest that dissolution testing in medium with 1.0% w/v SLS and a 30 minute endpoint is predictive of the in vivo performance. However, the dissolution testing in medium with 2.0% w/v SLS was not able to predict the in vivo performance differences due to the drug substance particle size changes.

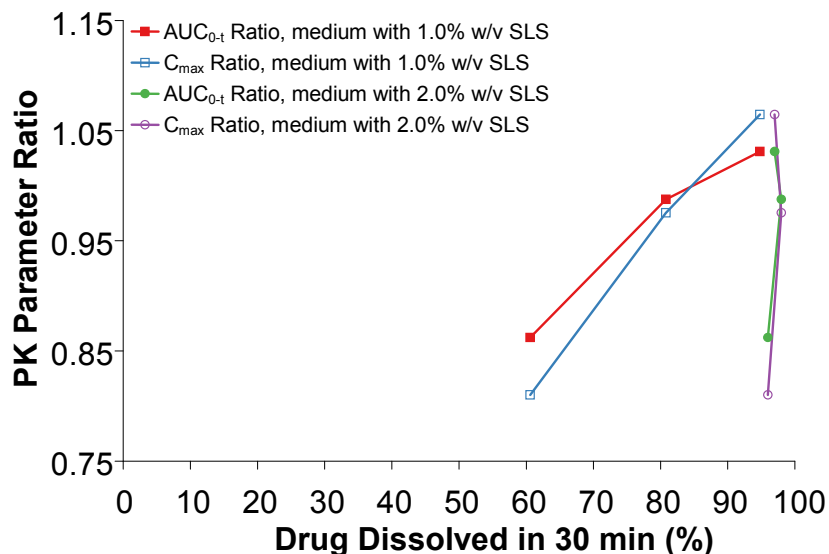


Figure 6. AUC_{0-t} ratio and C_{max} ratio as a function of the percentage of drug dissolved in 30 minutes

A dissolution rate of not less than (NLT) 80% in 30 minutes in 0.1 N HCl with 1.0% w/v SLS was set as the target for pharmaceutical development studies based on the fact that Batch 19 (d₉₀ 30 μm) showed 80.8% dissolution in 30 minutes and demonstrated comparable pharmacokinetic profiles to the RLD in the pilot BE study.

2.1 Components of Drug Product

2.1.1 Drug Substance

2.1.1.1 Physical Properties

Physical description:

The following physical description is for acetriptyan Form III.

Appearance: White to off-white, crystalline powder

Particle morphology: Plate-like crystals

Particle size distribution: PSD of drug substance Lot #2 was measured using Malvern Mastersizer. The results were as follows: d₁₀ – 7.2 μm; d₅₀ – 12 μm; d₉₀ – 20 μm. This is representative of the drug substance PSD selected for the final drug product formulation.

Solid state form:

To date, three different crystalline forms (Form I, II and III) have been identified and reported in the literature. The three different forms were prepared using different solvents and crystallization conditions. The solubility and the melting point are different for each of the three polymorphs. Polymorphic Form III is the most stable form and has the highest melting point. The DMF holder provides acetriptyan polymorphic Form III consistently based on in-house batch analysis data

obtained by XRPD and DSC. Stress testing confirmed that no polymorphic conversion was observed (Table 10) and Form III is stable under the stress conditions of high temperatures, high humidity, UV light and mechanical stress. Since it is the most stable form, no phase transformation during the manufacturing process is expected. The Form III melting point and characteristic 2θ values are included in the drug substance specification as a part of the control strategy.

To confirm its physical stability, the final drug product was sampled during lab scale studies to evaluate whether processing conditions affected the polymorphic form of the drug substance. The XRPD data showed that the characteristics 2θ peaks of Form III of the drug substance are retained in the final drug product. Representative profiles are shown in Figure 7. An advanced XRPD technique was utilized to detect the possible phase transition in the drug product since the level of drug substance was 10% in the drug product.

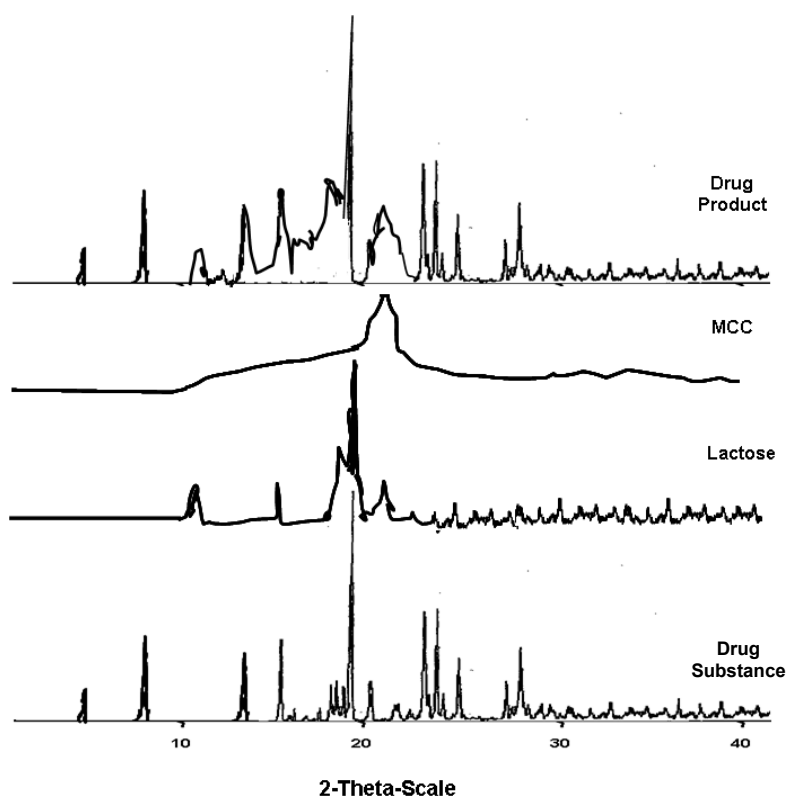


Figure 7. The XRPD profiles of drug product, MCC, lactose and drug substance

The most stable polymorph (Form III) exhibits plate-like morphology as shown in Figure 8.

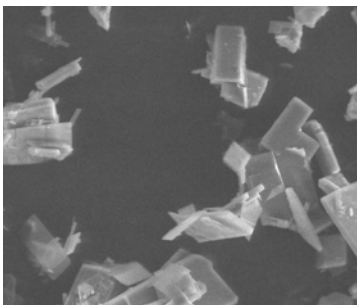


Figure 8. SEM picture of acetriptan

Melting point: Approximately 186 °C (Form III)

Aqueous solubility as a function of pH:

The solubility of acetriptan Form III in aqueous media as a function of pH was measured and is presented in Table 9. The aqueous solubility of acetriptan is low (~0.015 mg/mL) and constant across the physiological pH range due to the lipophilic nature of the molecule.

Table 9. Solubility of acetriptan Form III in various media with different pH

Media	Solubility
--	(mg/mL)
0.1 N HCl	0.015
pH 4.5 buffer	0.015
pH 6.8 buffer	0.015

Hygroscopicity:

Acetriptan Form III is non-hygroscopic and requires no special protection from humidity during handling, shipping or storage. Hygroscopicity studies were carried out using a vapor sorption analyzer. The temperature was maintained at 25 °C. The material was exposed to stepwise increases in relative humidity from 10% to 90% for up to 150 minutes at each condition. The drug substance was non-hygroscopic, adsorbing less than 0.2% w/w at 90% RH.

Density (Bulk, Tapped, and True) and Flowability:

The bulk, tapped and true density as well as the flowability of acetriptan Form III (Lot #2 : $d_{10} - 7.2 \mu\text{m}$; $d_{50} - 12 \mu\text{m}$; $d_{90} - 20 \mu\text{m}$) were measured.

Bulk density: 0.27 g/cc

Tapped density: 0.39 g/cc

True density: 0.55 g/cc

The flow function coefficient (ffc) was 2.95 and the Hausner ratio was 1.44 which both indicate poor flow properties. The cohesiveness of the drug substance was also studied using a powder rheometer. The specific energy (12 mJ/g) of the drug substance indicates that the drug substance is cohesive.

2.1.1.2 Chemical Properties

pKa: Acetripitan is a weak base with a pKa of 9.2.

Chemical stability in solid state and in solution:

Stress testing (forced degradation) was carried out on acetripitan to study its impurity profile, degradation pathway and to facilitate the development of a stability-indicating method. In addition, knowledge obtained from the forced degradation studies was used during formulation and process design and development to prevent impurities from being generated. The specified stress conditions were intended to achieve approximately 5-20% degradation (if possible) of acetripitan or to represent a typical stress condition even though less than 5% degradation was achieved due to its inherent stability. The stressed samples were compared to the unstressed sample (control). Stress conditions and results are listed in Table 10 below.

Table 10. Acetripitan Form III stability under stress conditions

Stress Conditions	Assay (% w/w)	Degradation Products (% w/w)				Solid State Form
		RC1	RC2	RC3	RC4	
Untreated	99.4	ND	ND	ND	ND	Crystalline Form III
Saturated Solution						
0.1 N HCl (RT, 14 days)	96.9	ND	2.3	1.1	ND	N/A
0.1 N NaOH (RT, 14 days)	97.3	ND	2.1	0.9	ND	N/A
3% H ₂ O ₂ (RT, 7 days)	86.7	ND	9.9	1.3	ND	N/A
Purified water (RT, 14 days)	96.8	ND	1.9	1.2	ND	N/A
Photostability (ICH Q1B Option 1)	90.6	ND	7.5	2.1	ND	N/A
Heat (60 °C, 24 h)	93.4	ND	5.2	ND	1.5	N/A
Solid State Material						
Humidity (open container, 90% RH, 25 °C, 7 days)	99.4	ND	0.1	0.1	ND	No change
Humidity and heat (open container, 90% RH, 40 °C, 7 days)	99.9	ND	0.1	0.1	ND	No change
Humidity and heat (open container, 90% RH, 60 °C, 7 days)	95.9	ND	2.7	0.2	1.4	No change
Photostability (ICH Q1B Option 1)	95.5	ND	3.2	1.4	ND	No change
Dry heat (60 °C, 7 days)	95.8	ND	4.1	ND	0.9	No change
Dry heat (105 °C, 96 h)	82.5	ND	3.9	ND	13.7	No change
Mechanical stress (Grinding and compression)	99.2	ND	0.1	0.1	ND	No change

ND: Not Detected; N/A: Not Applicable

Samples were analyzed by HPLC equipped with a peak purity analyzer (photodiode array). Degradation peaks were well resolved from the main peak (acetripitan). The peak purity of the main peak and monitored degradants RC2 (ACE12345), RC3 (RRT = 0.68) and RC4 (RRT=0.79) were greater than 0.99. For each degradant, the peak purity angle was less than the peak purity threshold, suggesting that there was no interference of degradants with the main

peak. Degradant RC1 was not observed. Degradant RC2 was formed due to oxidation and degradant RC3 was the result of further oxidation. Based on the results of the forced degradation studies, RC2 and RC3 were identified as the principal degradation products under the stress conditions. RC3 was not found under long-term stability conditions. With prolonged exposure to excessive high temperature (105 °C, 96 hours), 14% of RC4 was observed.

Overall, acetriptan is susceptible to dry heat, UV light and oxidative degradation.

2.1.1.3 Biological Properties

Partition coefficient: Log P 3.55 (25 °C, pH 6.8)

Caco-2 permeability: 34×10^{-6} cm/s

The Caco-2 permeability is higher than the reference standard, metoprolol, which has a Caco-2 permeability of 20×10^{-6} cm/s. Therefore, acetriptan is highly permeable.

Biopharmaceutics Classification:

Literature and in-house experimental data support the categorization of acetriptan as a highly permeable drug substance. Based on its solubility across physiological pH (Table 9) acetriptan is designated as a low solubility drug substance. The calculated dose solubility volume is as follows:

$$20 \text{ mg (highest strength)} / (0.015 \text{ mg/mL}) = 1333 \text{ mL} > 250 \text{ mL}$$

Therefore, acetriptan is considered a BCS Class II compound (low solubility and high permeability) according to the BCS guidance.

2.1.1.4 Risk Assessment of Drug Substance Attributes

A risk assessment of the drug substance attributes was performed to evaluate the impact that each attribute could have on the drug product CQAs. The outcome of the assessment and the accompanying justification is provided as a summary in the pharmaceutical development report. The relative risk that each attribute presents was ranked as high, medium or low. The high risk attributes warranted further investigation whereas the low risk attributes required no further investigation. The medium risk is considered acceptable based on current knowledge. Further investigation for medium risk may be needed in order to reduce the risk. The same relative risk ranking system was used throughout pharmaceutical development and is summarized in Table 11. For each risk assessment performed, the rationale for the risk assessment tool selection and the details of the risk identification, analysis and evaluation are available to the FDA Reviewer upon request.

Table 11. Overview of Relative Risk Ranking System

Low	Broadly acceptable risk. No further investigation is needed.
Medium	Risk is acceptable. Further investigation may be needed in order to reduce the risk.
High	Risk is unacceptable. Further investigation is needed to reduce the risk.

Note to Reader: According to ICH Q9 Quality Risk Management, it is important to note that “it is neither always appropriate nor always necessary to use a formal risk management process (using recognized tools and/or internal procedures e.g., standard operating procedures). The use of informal risk management processes (using empirical tools and/or internal procedures) can also be considered acceptable. Appropriate use of quality risk management can facilitate but does not obviate industry’s obligation to comply with regulatory requirements and does not replace appropriate communications between industry and regulators.”⁴

The two primary principles should be considered when implementing quality risk management:

- The evaluation of the risk to quality should be based on scientific knowledge and ultimately link to the protection of the patient; and*
- The level of effort, formality and documentation of the quality risk management process should be commensurate with the level of risk.*

Based upon the physicochemical and biological properties of the drug substance, the initial risk assessment of drug substance attributes on drug product CQAs is shown in Table 12.

Table 12. Initial risk assessment of the drug substance attributes

Drug Product CQAs	Drug Substance Attributes								
	Solid State Form	Particle Size Distribution (PSD)	Hygroscopicity	Solubility	Moisture Content	Residual Solvents	Process Impurities	Chemical Stability	Flow Properties
Assay	Low	Medium	Low	Low	Low	Low	Low	High	Medium
Content Uniformity	Low	High	Low	Low	Low	Low	Low	Low	High
Dissolution	High	High	Low	High	Low	Low	Low	Low	Low
Degradation Products	Medium	Low	Low	Low	Low	Low	Low	High	Low

The justification for the assigned level of risk is provided in Table 13.

⁴ ICH Harmonised Tripartite Guideline: Q9 Quality Risk Management. November 2005.

Table 13. Justification for the initial risk assessment of the drug substance attributes

Drug Substance Attributes	Drug Products CQAs	Justification
Solid State Form	Assay	Drug substance solid state form does not affect tablet assay and CU. The risk is low.
	Content Uniformity	
	Dissolution	Different polymorphic forms of the drug substance have different solubility and can impact tablet dissolution. The risk is high. Acetripitan polymorphic Form III is the most stable form and the DMF holder consistently provides this form. In addition, pre-formulation studies demonstrated that Form III does not undergo any polymorphic conversion under the various stress conditions tested. Thus, further evaluation of polymorphic form on drug product attributes was not conducted.
	Degradation Products	Drug substance with different polymorphic forms may have different chemical stability and may impact the degradation products of the tablet. The risk is medium.
Particle Size Distribution (PSD)	Assay	A small particle size and a wide PSD may adversely impact blend flowability. In extreme cases, poor flowability may cause an assay failure. The risk is medium.
	Content Uniformity	Particle size distribution has a direct impact on drug substance flowability and ultimately on CU. Due to the fact that the drug substance is milled, the risk is high.
	Dissolution	The drug substance is a BCS class II compound; therefore, PSD can affect dissolution. The risk is high.
	Degradation Products	The effect of particle size reduction on drug substance stability has been evaluated by the DMF holder. The milled drug substance exhibited similar stability as unmilled drug substance. The risk is low.
Hygroscopicity	Assay	Acetripitan is not hygroscopic. The risk is low.
	Content Uniformity	
	Dissolution	
	Degradation Products	
Solubility	Assay	Solubility does not affect tablet assay, CU and degradation products. Thus, the risk is low.
	Content Uniformity	
	Degradation Products	
	Dissolution	Acetripitan exhibited low (~0.015 mg/mL) and constant solubility across the physiological pH range. Drug substance solubility strongly impacts dissolution. The risk is high. Due to pharmaceutical equivalence requirements, the free base of the drug substance must be used in the generic product. The formulation and manufacturing process will be designed to mitigate this risk.
Moisture Content	Assay	Moisture is controlled in the drug substance specification (NMT 0.3%). Thus, it is unlikely to impact assay, CU and dissolution. The risk is low.
	Content Uniformity	
	Dissolution	
	Degradation Products	The drug substance is not sensitive to moisture based on forced degradation studies. The risk is low.

Drug Substance Attributes	Drug Products CQAs	Justification
Residual Solvents	Assay	Residual solvents are controlled in the drug substance specification and comply with USP <467>. At ppm level, residual solvents are unlikely to impact assay, CU and dissolution. The risk is low.
	Content Uniformity	
	Dissolution	
	Degradation Products	There are no known incompatibilities between the residual solvents and acetriptan or commonly used tablet excipients. As a result, the risk is low.
Process Impurities	Assay	Total impurities are controlled in the drug substance specification (NMT 1.0%). Impurity limits comply with ICH Q3A recommendations. Within this range, process impurities are unlikely to impact assay, CU and dissolution. The risk is low.
	Content Uniformity	
	Dissolution	
	Degradation Products	During the excipient compatibility study, no incompatibility between process impurities and commonly used tablet excipients was observed. The risk is low.
Chemical Stability	Assay	The drug substance is susceptible to dry heat, UV light and oxidative degradation; therefore, acetriptan chemical stability may affect drug product assay and degradation products. The risk is high.
	Content Uniformity	Tablet CU is mainly impacted by powder flowability and blend uniformity. Tablet CU is unrelated to drug substance chemical stability. The risk is low.
	Dissolution	Tablet dissolution is mainly impacted by drug substance solubility and particle size distribution. Tablet dissolution is unrelated to drug substance chemical stability. The risk is low.
	Degradation Products	The risk is high. See justification for assay.
Flow Properties	Assay	Acetriptan has poor flow properties. In extreme cases, poor flow may impact assay. The risk is medium.
	Content Uniformity	Acetriptan has poor flow properties which may lead to poor tablet CU. The risk is high.
	Dissolution	The flowability of the drug substance is not related to its degradation pathway or solubility. Therefore, the risk is low.
	Degradation Products	

2.1.2 Excipients

The excipients used in acetriptan tablets were selected based on the excipients used in the RLD, excipient compatibility studies and prior use in approved ANDA products that utilize roller compaction (RC). A summary of the excipient-drug substance compatibility studies and the selection of each excipient grade is provided in the following section.

2.1.2.1 Excipient Compatibility Studies

Note to Reader: Excipient compatibility is an important part of understanding the role of inactive ingredients in product quality. The selection of excipients for the compatibility study should be based on the mechanistic understanding of the drug substance and its impurities, excipients and their impurities, degradation pathway and potential processing conditions for the drug product manufacture. A scientifically sound approach should be used in constructing the compatibility studies. The commercial grades of the excipients are not provided in this example

to avoid endorsement of specific products. However, in an actual pharmaceutical development report, the names of the commercial grades are expected.

Excipient-drug substance compatibility was assessed through HPLC analysis of binary mixtures of excipient and drug substance at a 1:1 ratio in the solid state. Samples were stored at 25 °C/60 % RH and 40 °C/75 % RH in both open and closed containers for 1 month. Common excipients functioning as filler, disintegrant, and lubricant were evaluated in the excipient compatibility study. Table 14 summarizes the results.

Table 14. Excipient compatibility (binary mixtures)*

Mixture	Assay	Degradants
	(% w/w)	(% w/w)
Lactose Monohydrate/DS (1:1)	99.8%	ND
Lactose Anhydrous/DS (1:1)	99.6%	ND
Microcrystalline Cellulose (MCC)/DS (1:1)	98.4%	ND
Dibasic Calcium Phosphate/DS (1:1)	99.3%	ND
Mannitol/DS (1:1)	101.1%	ND
Pregelatinized Starch/DS (1:1)	100.5%	ND
Croscarmellose Sodium (CCS)/DS (1:1)	99.7%	ND
Crospovidone (1:1)	99.3%	ND
Sodium Starch Glycolate (1:1)	98.8%	ND
Talc/DS (1:1)	99.5%	ND
Magnesium Stearate/DS (1:1)	95.1%	AD1: 4.4%

*Conditions: 40 °C/75 % RH, open container, 1 month

Loss in assay or detection of degradants indicative of an incompatibility was not observed for the selected excipients except magnesium stearate. An interaction was seen with magnesium stearate at 40 °C/75 % RH. This interaction caused lower assay results for acetriptyan. The mechanism for this interaction was indentified as formation of a magnesium stearate-acetriptyan adduct (AD1) involving stearic acid. To further evaluate if this potential interaction could cause drug instability, an additional experiment was performed in which several different mixtures of drug and excipients were prepared. Only the excipient types used in the RLD formulation were selected for this study. The first mixture consisted of drug and all excipients in the ratio representative of the finished product. In subsequent mixtures, one excipient was removed at a time. These mixtures were stored at 25 °C/60% RH and 40 °C/75% RH in both open and closed containers for 1 month. Table 15 presents the results of the study.

Table 15. Excipient compatibility (interaction study)*

Mixture	Assay	Degradants
	(% w/w)	(% w/w)
All excipients	99.4%	ND
All excipients except Lactose Monohydrate	99.2%	ND
All excipients except Microcrystalline Cellulose (MCC)	99.8%	ND
All excipients except Croscarmellose Sodium (CCS)	99.9%	ND
All excipients except Talc	99.3%	ND
All excipients except Magnesium Stearate	99.6%	ND

*Conditions: 40 °C/75 % RH, open container, 1 month

No loss in assay was observed in any of these mixtures at 40 °C/75% RH or at 25 °C/60% RH. There is no incompatibility with the selected excipients except for the noted interaction with magnesium stearate in the binary mixture study. Therefore, magnesium stearate was still selected, but contact of the drug substance with magnesium stearate was limited by only using extragranular magnesium stearate. Intragranular lubrication required for the roller compaction process was achieved by using talc. Subsequent assurance of compatibility was provided by long-term stability data for formulations used in the pilot BE study and the ongoing prototype stability studies using the formulation proposed for commercialization. The impurity method is able to identify and quantify AD1. Adduct formation was below the limit of quantitation in the long-term stability study and is controlled by the limit for any unspecified impurity.

2.1.2.2 Excipient Grade Selection

Based on the results of excipient compatibility studies, identical excipient types to the RLD formulation were selected for the generic product development. The selection of excipient grade and supplier was based on previous formulation experience and knowledge about excipients that have been used successfully in approved products manufactured by roller compaction as given in Table 16. The level of excipients used in the formulation were studied in subsequent formulation development studies.

Table 16. Initial selection of excipient type, grade and supplier

Excipient	Supplier	Grade	Prior Use in Roller Compaction
Lactose Monohydrate	A	A01	ANDA 123456, ANDA 456123
Microcrystalline Cellulose (MCC)	B	B02	ANDA 123456, ANDA 456123
Croscarmellose Sodium (CCS)	C	C03	ANDA 123456
Talc	D	D04	ANDA 123456
Magnesium Stearate	E	E05	ANDA 123456, ANDA 456123

Microcrystalline cellulose and lactose monohydrate comprise about 80% of the total drug product composition. Microcrystalline cellulose and lactose monohydrate are among the commonly used fillers for dry granulation formulations, both individually and in combination with each other, because they exhibit appropriate flow and compression properties. The particle size distribution, particle morphology, aspect ratio, bulk density and flowability of different grades have the potential to affect drug product content uniformity. Therefore, additional particle size controls above those in the pharmacopoeia are included in the specifications for the two major excipients: lactose monohydrate (d_{50} : 70-100 μm) and microcrystalline cellulose (d_{50} : 80-140 μm). Material within these ranges was used in all further formulation studies.

Lactose Monohydrate: Lactose monohydrate is commonly used as a filler. The potential impurities of lactose are melamine and aldehydes. The supplier has certified that the lactose is free of melamine and has provided a certificate of suitability for TSE/BSE. Lactose monohydrate Grade A01 from supplier A was selected based on successful product development in approved ANDA 123456 and ANDA 456123, both of which used roller compaction. The selected grade provides acceptable flow and compression properties when used in combination with microcrystalline cellulose.

Microcrystalline Cellulose (MCC): Microcrystalline cellulose is widely used as a filler for direct compression and roller compaction. Though it is reported in the literature that MCC may physically bind or adsorb drug substance, no such physical interaction was evident in the formulation dissolution studies. It is known from the literature that MCC undergoes plastic deformation during compaction since it is a fibrous material and ductile in nature. Not all grades of MCC may be suitable for use in roller compaction. Microcrystalline cellulose Grade B02 from supplier B was selected based on the acceptable flow and compression properties when used in combination with lactose monohydrate as demonstrated in approved ANDA 123456 and ANDA 456123.

Croscarmellose Sodium (CCS): Acetripitan is a BCS class II drug so rapid disintegration is necessary to ensure maximum bioavailability. Being a superdisintegrant, croscarmellose sodium is hygroscopic in nature. It swells rapidly to about 4-8 times its original volume when it comes in contact with water. Grade C03 from supplier C was selected.

Talc: Talc is a common metamorphic mineral and is used as a glidant and/or lubricant both intragranularly and extragranularly in the formulation. Intragranular talc was used to prevent sticking during the roller compaction process. Because of the interaction between magnesium stearate and acetripitan, talc was also added extragranularly to reduce the level of magnesium stearate needed for the lubrication. Grade D04 from supplier D was selected.

Magnesium Stearate: It is the most commonly used lubricant for tablets. Because magnesium stearate interacts with acetripitan to form an adduct, it is used only extragranularly. Magnesium stearate grade E05 from supplier E was selected and is of vegetable origin.

2.2 Drug Product

2.2.1 Formulation Development

2.2.1.1 Initial Risk Assessment of the Formulation Variables

Note to Reader: In this initial risk assessment for formulation development, the detailed manufacturing process has not been established. Thus, risks were rated assuming that for each formulation attribute that changed, an optimized manufacturing process would be established.

The results of the initial risk assessment of the formulation variables are presented in Table 17 and the justification for the risk assignment is presented in Table 18.

Table 17. Initial risk assessment of the formulation variables

Drug Product CQA	Formulation Variables				
	Drug Substance PSD	MCC/Lactose Ratio	CCS Level	Talc Level	Magnesium Stearate Level
Assay	Medium	Medium	Low	Low	Low
Content Uniformity	High	High	Low	Low	Low
Dissolution	High	Medium	High	Low	High
Degradation Products	Low	Low	Low	Low	Medium

Table 18. Justification for the initial risk assessment of the formulation variables

Formulation Variables	Drug Products CQAs	Justification
Drug Substance PSD	Assay	See Justifications provided in Table 13.
	Content Uniformity	
	Dissolution	
	Degradation Products	
MCC/Lactose Ratio	Assay	MCC/Lactose ratio can impact the flow properties of the blend. This, in turn, can impact tablet CU. The risk is high.
	Content Uniformity	Occasionally, poor CU can also adversely impact assay. The risk is medium.
	Dissolution	MCC/lactose ratio can impact dissolution via tablet hardness. However, hardness can be controlled during compression. The risk is medium.
	Degradation Products	Since both MCC and lactose are compatible with the drug substance and will not impact drug product degradation, the risk is low.
CCS Level	Assay	Since the level of CCS used is low and its impact on flow is minimal, it is unlikely to impact assay and CU. The risk is low.
	Content Uniformity	
	Dissolution	CCS level can impact the disintegration time and, ultimately, dissolution. Since achieving rapid disintegration is important for a drug product containing a BCS class II compound, the risk is high.
	Degradation Products	CCS is compatible with the drug substance and will not impact drug product degradation. Thus, the risk is low.
Talc Level	Assay	Generally, talc enhances blend flowability. A low level of talc is not likely to impact assay and CU. The risk is low.
	Content Uniformity	
	Dissolution	Compared to magnesium stearate, talc has less impact on disintegration and dissolution. The low level of talc used in the formulation is not expected to impact dissolution. The risk is low.
	Degradation Products	Talc is compatible with the drug substance and will not impact degradation products. The risk is low.

Formulation Variables	Drug Products CQAs	Justification
Magnesium Stearate Level	Assay	Since the level of magnesium stearate used is low and its impact on flow is minimal, it is unlikely to impact assay and CU. The risk is low.
	Content Uniformity	
	Dissolution	Over-lubrication due to excessive lubricant may retard dissolution. The risk is high.
	Degradation Products	Though it formed an adduct with the drug substance in the binary mixture compatibility study (magnesium stearate/DS ratio 1:1), the interaction compatibility study showed that the adduct formation is negligible when magnesium stearate is used at a level representative of the finished drug product composition (magnesium stearate/DS ratio 1:10). Thus, the risk is medium.

2.2.1.2 Drug Substance Particle Size Selection for Product Development

In general, for drug substance with plate-like morphology and particle size in the micrometer range, a larger drug substance particle size improves manufacturability because it has better flow. However, for a BCS II compound like acetriptan, larger drug substance particle size may significantly decrease dissolution and negatively impact the in vivo performance. With an aim to identify the appropriate drug substance particle size distribution range for further study, an in silico simulation was conducted to estimate the impact of the drug substance mean particle size, d_{50} , on the C_{max} ratio and AUC ratio between the test product and the RLD.⁵ The predefined selection criterion was a mean particle size that yielded both a C_{max} ratio and an AUC ratio between 0.9 and 1.11. The result of the simulation for d_{50} ranging from 1 μm to 200 μm is presented graphically in Figure 9. The data indicate that a d_{50} of 30 μm or less met the predefined criterion and exhibited a limited effect on the pharmacokinetic profile when compared to the RLD.

⁵ W. Huang, S. Lee and L.X. Yu. Mechanistic Approaches to Predicting Oral Drug Absorption. The AAPS Journal, 2009, 11(2): 217-224.

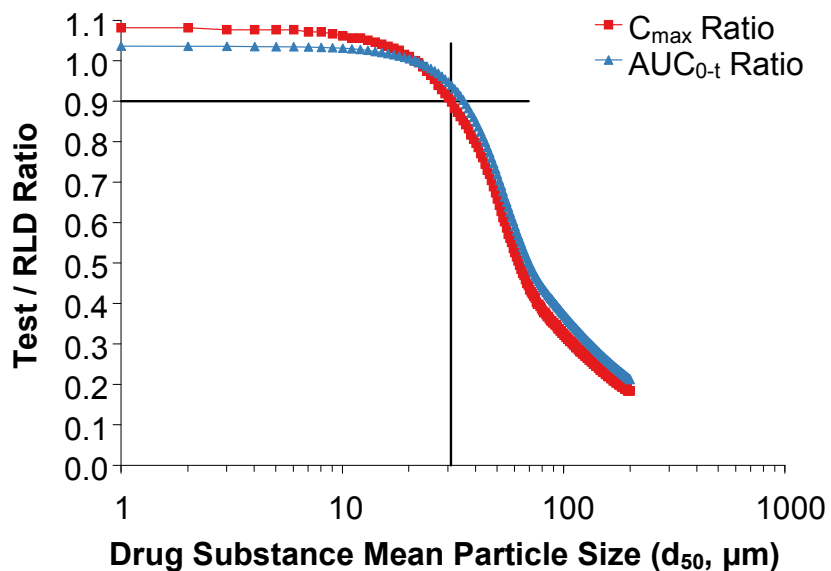


Figure 9. In silico simulation of pharmacokinetic profiles versus drug substance mean particle size

Based on the results of the simulation, drug substance lots with four different particle size distributions were selected for formulation development. Ultimately, the goal was to test the formulations in a pilot PK study to finalize the drug substance particle size distribution for commercialization. Both physical and flow properties of the four drug substance lots were evaluated and are summarized in Table 19. In this development report, d_{90} is used to describe the drug substance particle size distribution. The acetriptan d_{90} of 10 μm , 20 μm , 30 μm and 45 μm correspond to a d_{50} of 6 μm , 12 μm , 24 μm and 39 μm , respectively.

Table 19. Drug substance lots used for formulation development

Physical Properties	Interpretation of Data	Lot #1	Lot #2	Lot #3	Lot #4
d_{90} (μm)	--	10	20	30	45
d_{50} (μm)	--	6	12	24	39
d_{10} (μm)	--	3.6	7.2	14.4	33.4
Bulk density (g/cc)	--	0.26	0.27	0.28	0.29
Tapped density (g/cc)	--	0.41	0.39	0.39	0.38
Flow function coefficient (ffc) ⁶	ffc < 3.5 poor flow 3.5 < ffc < 5.0 marginal flow 5.0 < ffc < 8.0 good flow ffc > 8.0 excellent flow	2.88	2.95	3.17	3.21
Compressibility index (%) ⁷	< 15 good flow	36.6	30.8	28.2	23.7
Hausner ratio ⁷	< 1.25 fair flow	1.58	1.44	1.39	1.31
Specific energy (mJ/g) determined by powder rheometer ⁸	5 < SE < 10 moderate cohesion SE > 10 high cohesion	13	12	10	8.5

2.2.1.3 Process Selection

When d_{90} is in the range of 10-45 μm , acetriptan is cohesive and displays poor flowability as evidenced by the compressibility index, Hausner ratio, flow function coefficient and specific energy. Poor material flow may produce tablets with high weight and content variability due to an uneven distribution of the drug substance in the blend, uneven bulk density and, eventually, uneven filling of die cavities on the tablet press. Poor acetriptan flow rules out the use of a high drug load formulation and supports the use of a similar drug load to the RLD which is 10%.

Initially, direct compression of the blend was performed. The blend uniformity (BU) percent relative standard deviation (% RSD) was higher than 6% and the tablet content uniformity % RSD was even higher. Therefore, direct compression was considered an unacceptable process for this formulation.

Wet granulation was excluded due to potential thermal degradation of the drug substance during drying based on the forced degradation study results. The use of wet granulation with an organic solvent was also excluded because of the desire to avoid the environmental considerations involved. For dry granulation by roller compaction, the powder particles of drug substance and fillers are aggregated under high pressure to form a ribbon and then broken down to produce granules by milling before compression (tableting). The risk of drug particle segregation can be minimized. By controlling the size distribution and flow properties of the granules, the risk of poor tablet content uniformity can be reduced. Thus, dry granulation by roller compaction was selected as the process for further drug product development efforts.

⁶ M. P. Mullarney and N. Leyva, Modeling Pharmaceutical Powder-Flow Performance Using Particle-Size Distribution Data, *Pharmaceutical Technology*, 2009, 33(3): 126-134.

⁷ The full scale of flowability for compressibility index and Hausner ratio are provided in USP <1174> Powder Flow.

⁸ As per powder rheometer equipment vendor guideline

2.2.1.4 Formulation Development Study #1

Note to Reader: A univariate method (i.e., one-factor-at-a time (OFAT)) is acceptable in cases where there is no potential interaction between factors. Since this is often not known, a multivariate statistical design (i.e., Design of Experiments (DOE)) is often used and results are evaluated with commercially available statistical software. A sequential strategy is commonly employed when planning a DOE. Initially, a screening DOE can be used to narrow down the extensive list of factors identified during initial risk assessment to a few vital factors. Then, a characterization DOE can be used to understand the main effects and potential interaction(s) between these vital factors. When center points are included in a 2-level factorial DOE, it is possible to test if the curvature effect is significant. Data analysis is done by separating the curvature term from the regression model in an adjusted model. If the curvature is significant, the design should be augmented to a response surface DOE to estimate the quadratic terms. On the other hand, if the curvature is not significant, the adjusted model and unadjusted model will be similar. Finally, a verification DOE can be employed to study the robustness of the system by varying the identified critical factors over ranges that are expected to be encountered during routine manufacturing.

Randomization, blocking and replication are the three basic principles of statistical experimental design. By properly randomizing the experiment, the effects of uncontrollable factors that may be present can be “averaged out”. Blocking is the arrangement of experimental units into groups (blocks) that are similar to one another. Blocking reduces known but irrelevant sources of variation between groups and thus allows greater precision in the estimation of the source of variation under study. Replication allows the estimation of the pure experimental error for determining whether observed differences in the data are really statistically different.

In this mock example, we have not included ANOVA results for each DOE. In practice, please be advised that ANOVA results should accompany all DOE data analysis, especially if conclusions concerning the significance of the model terms are discussed.

For all DOE data analysis, the commonly used alpha of 0.05 was chosen to differentiate between significant and nonsignificant factors.

It is important that any experimental design has sufficient power to ensure that the conclusions drawn are meaningful. Power can be estimated by calculating the signal to noise ratio. If the power is lower than the desired level, some remedies can be employed to increase the power, for example, by adding more runs, increasing the signal or decreasing the system noise. Please refer to the ICH Points to Consider document for guidance on the level of DOE documentation recommended for regulatory submissions.⁹

Formulation development focused on evaluation of the high risk formulation variables as identified in the initial risk assessment shown in Table 17. The development was conducted in two stages. The first formulation study evaluated the impact of the drug substance particle size distribution, the MCC/Lactose ratio and the disintegrant level on the drug product CQAs. The

⁹ ICH Quality Implementation Working Group Points to Consider (R2). December 6, 2011.

second formulation study was conducted to understand the impact of extragranular magnesium stearate and talc level in the formulation on product quality and manufacturability. Formulation development studies were conducted at laboratory scale (1.0 kg, 5,000 units). Table 20 details the equipment and the associated process parameters used in these studies.

Table 20. Equipment and fixed process parameters used in formulation development studies

Process Step	Equipment
Pre-Roller Compaction Blending and Lubrication	4 qt V-blender <ul style="list-style-type: none"> ○ 250 revolutions for blending (10 min at 25 rpm)
Roller Compaction and Integrated Milling	Alexanderwerk ¹⁰ WP120 with 25 mm roller width and 120 mm roller diameter <ul style="list-style-type: none"> ○ Roller surface: Knurled ○ Roller pressure: 50 bar ○ Roller gap: 2 mm ○ Roller speed: 8 rpm ○ Mill speed: 60 rpm ○ Coarse screen orifice size: 2.0 mm ○ Mill screen orifice size: 1.0 mm
Final Blending and Lubrication	4 qt V-blender <ul style="list-style-type: none"> ○ 100 revolutions for granule and talc blending (4 min at 25 rpm) ○ 75 revolutions for lubrication (3 min at 25 rpm)
Tablet Compression	16-station rotary press (2 stations used) <ul style="list-style-type: none"> ○ 8 mm standard round concave tools ○ Press speed: 20 rpm ○ Compression force: 5-15 kN ○ Pre-compression force: 1 kN

The goal of Formulation Development Study #1 was to select the MCC/Lactose ratio and disintegrant level and to understand if there was any interaction of these variables with drug substance particle size distribution. This study also sought to establish the robustness of the proposed formulation. A 2³ full factorial Design of Experiments (DOE) with three center points was used to study the impact of these three formulation factors on the response variables listed in Table 21.

The acetriptan d₉₀ of 10 µm, 20 µm and 30 µm corresponds with the d₅₀ of 6 µm, 12 µm and 24 µm, respectively. These drug substance lots are characterized in Table 19 and were selected based on the in silico simulation results discussed in *Section 2.2.1.2*.

Disintegrant (croscarmellose sodium) was added intragranularly and the levels investigated ranged from 1% to 5%. These levels are consistent with the estimated level in the RLD formulation and are within the recommended range in the Handbook of Pharmaceutical Excipients.¹¹

¹⁰ FDA does not endorse any particular equipment vendors.

¹¹ Rowe, RC., PJ Sheskey and ME Quinn. Handbook of Pharmaceutical Excipients, 6th Edition. Grayslake, IL: RPS Publishing, 2009.

The MCC/Lactose ratios selected for formulation studies were based on experience with previously approved products manufactured using roller compaction (ANDA 123456 and ANDA 456123). The MCC/Lactose ratios are transformed to a continuous numeric variable as a percentage of MCC in the MCC/Lactose dual filler combination by assigning values of 33.3%, 50.0% and 66.7% corresponding to 1:2, 1:1 and 2:1, respectively.

The drug load in the generic formulation was fixed at 10% based on the RLD label, strength and tablet weight. For this study, both intragranular and extragranular talc levels were fixed at 2.5%. The extragranular magnesium stearate level was fixed at 1%. The levels of talc and magnesium stearate are consistent with the levels observed in the RLD formulation and agree with the recommendations published in the Handbook of Pharmaceutical Excipients.¹¹ A constant tablet weight of 200.0 mg was used with the filler amount adjusted to achieve the target weight.

Table 21 summarizes the factors and responses studied. For each batch, the blend was compressed at several compression forces (*data shown for only 5 kN, 10 kN and 15 kN*) to obtain the compression profile. Using the profile, the force was adjusted to compress tablets to the target hardness for disintegration and dissolution testing.

Table 21. Design of the 2³ full factorial DOE to study intragranular excipients and drug substance PSD

Factors: Formulation Variables		Levels		
		-1	0	+1
A	Drug substance PSD (d ₉₀ , µm)	10	20	30
B	Disintegrant (%)	1	3	5
C	% MCC in MCC/Lactose combination	33.3	50.0	66.7
Responses		Goal	Acceptable Ranges	
Y ₁	Dissolution at 30 min (%) (with hardness of 12.0 kP)	Maximize	≥ 80%	
Y ₂	Disintegration time (min) (with hardness of 12.0 kP)	Minimize	< 5 min	
Y ₃	Tablet content uniformity (% RSD)	Minimize % RSD	< 5%	
Y ₄	Assay (% w/w)	Target at 100% w/w	95.0-105.0% w/w	
Y ₅	Powder blend flow function coefficient (ffc)	Maximize	> 6	
Y ₆	Tablet hardness@ 5 kN (kP)	Maximize	> 5.0 kP	
Y ₇	Tablet hardness @ 10 kN (kP)	Maximize	> 9.0 kP	
Y ₈	Tablet hardness @ 15 kN (kP)	Maximize	> 12.0 kP	
Y ₉	Friability @ 5 kN (%)	Minimize	< 1.0%	
Y ₁₀	Friability @ 10 kN (%)	Minimize	< 1.0%	
Y ₁₁	Friability @ 15 kN (%)	Minimize	< 1.0%	
Y ₁₂	Degradation products (%) (observed at 3 months, 40 °C/75% RH)	Minimize	ACE12345: NMT 0.5% Any unknown impurity: NMT 0.2% Total impurities: NMT 1.0%	

To study tablet dissolution at a target tablet hardness of 12.0 kP (a range of 11.0-13.0 kP was allowed), the compression force was adjusted. A target tablet hardness of 12.0 kP was chosen to investigate the effect of formulation variables on dissolution because a high hardness would be expected to be the worst case for dissolution. If dissolution was studied at a fixed compression force, the results could be confounded by the impact of tablet hardness.

The flow function coefficient (ffc) of the powder blend prior to roller compaction (Y_6) was measured using a ring shear tester. According to the literature⁶, the following rule is used to gauge the powder's relative flowability:

- ffc < 3.5 poor
- 3.5 < ffc < 5.0 marginal
- 5.0 < ffc < 8.0 good
- ffc > 8.0 excellent

The experimental results for dissolution, content uniformity, powder blend flow function coefficient and tablet hardness when compressed at 10 kN (Y_1 , Y_3 , Y_5 and Y_7 , other responses not shown) are presented in Table 22.

Table 22. Experimental results of the DOE to study intragranular excipients and drug substance PSD

Batch No.	Factors: Formulation Variables			Responses			
	A: Drug substance PSD	B: Disintegrant level	C: % MCC in MCC/Lactose combination	Y_1 : Dissolution at 30 min	Y_3 : CU	Y_5 : ffc value	Y_7 : Tablet hardness @ 10 kN
	(d_{90} , μm)	(%)	(%)	(%)	(% RSD)	--	(kP)
1	30	1	66.7	76.0	3.8	7.56	12.5
2	30	5	66.7	84.0	4.0	7.25	13.2
3	20	3	50.0	91.0	4.0	6.62	10.6
4	20	3	50.0	89.4	3.9	6.66	10.9
5	30	1	33.3	77.0	2.9	8.46	8.3
6	10	5	66.7	99.0	5.1	4.77	12.9
7	10	1	66.7	99.0	5.0	4.97	13.5
8	20	3	50.0	92.0	4.1	6.46	11.3
9	30	5	33.3	86.0	3.2	8.46	8.6
10	10	1	33.3	99.5	4.1	6.16	9.1
11	10	5	33.3	98.7	4.0	6.09	9.1

Significant factors for tablet dissolution (at 30 min)

Initially, dissolution was tested using the FDA-recommended method. All batches exhibited rapid and comparable dissolution (> 90% dissolved in 30 min) to the RLD. All batches were then retested using the in-house dissolution method (see details in Section 1.4). Results are presented in Table 22. Since center points were included in the DOE, the significance of the curvature effect was tested using an adjusted model. The Analysis of Variance (ANOVA) results are presented in Table 23.

Table 23. ANOVA results of the model adjusted for curvature effect

Source	Sum of Squares	df*	Mean Square	F Value	p-value	Comments
Model	742.19	3	247.40	242.94	< 0.0001	Significant
A-Drug substance PSD (d ₉₀ , μm)	669.78	1	669.78	657.72	< 0.0001	Significant
B-Disintegrant (%)	32.81	1	32.81	32.21	0.0013	
AB-interaction	39.61	1	39.61	38.89	0.0008	
Curvature	1.77	1	1.77	1.74	0.2358	Not significant
Residual	6.11	6	1.02	--	--	--
Lack of Fit	2.67	4	0.67	0.39	0.8090	Not significant
Pure Error	3.44	2	1.72	--	--	--
Total	750.07	10	--	--	--	--

*df: degrees of freedom

As shown in Table 23, the curvature effect was not significant for dissolution; therefore, the factorial model coefficients were fit using all of the data (including center points). As shown in the following half-normal plot (Figure 10) and ANOVA results of the unadjusted model (Table 24), the significant factors affecting tablet dissolution were A (drug substance PSD), B (disintegrant level) and AB (an interaction between drug substance PSD and the intragranular disintegrant level).

Table 24. ANOVA results of the unadjusted model

Source	Sum of Squares	df	Mean Square	F Value	p-value	Comments
Model	742.19	3	247.40	219.84	< 0.0001	Significant
A-Drug substance PSD (d ₉₀ , μm)	669.78	1	669.78	595.19	< 0.0001	Significant
B-Disintegrant (%)	32.81	1	32.81	29.15	0.0010	
AB-Interaction	39.61	1	39.61	35.19	0.0006	
Residual	7.88	7	1.13	--	--	--
Lack of Fit	4.44	5	0.89	0.52	0.7618	Not significant
Pure Error	3.44	2	1.72	--	--	--
Total	750.07	10	--	--	--	--

Dissolution at 30 min (%)

Shapiro-Wilk Test
W-value = 0.926
p-value = 0.572

A: DS PSD (d_{90} , μm)
B: Disintegrant (%)
C: % MCC in MCC/Lactose
Combination

▲ Error Estimates
■ Positive Effects
■ Negative Effects

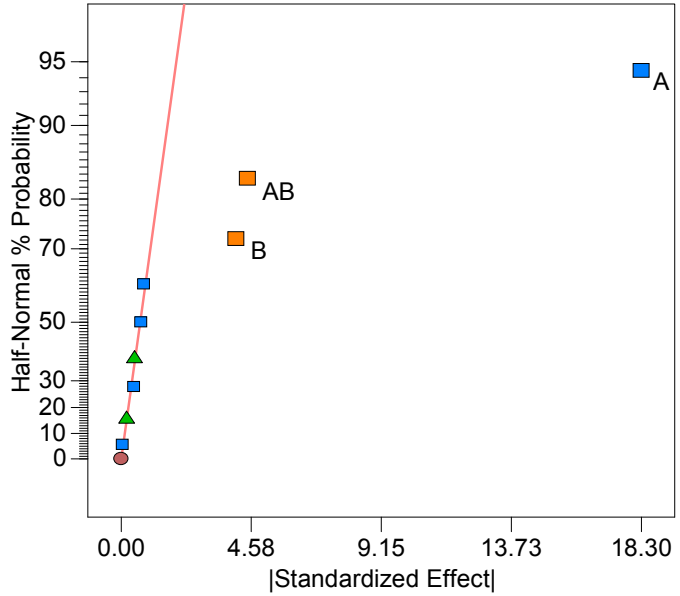


Figure 10. Half-normal plot of the formulation variable effects on dissolution at 30 min (tablet target hardness of 12.0 kP)

Figure 11 shows the effect of drug substance PSD and disintegrant level on dissolution at 30 minutes. Dissolution decreased with increasing drug substance PSD. On the other hand, dissolution increased with increasing disintegrant level. With a larger drug substance PSD, the disintegrant level had a greater impact on dissolution than with a smaller drug substance PSD.

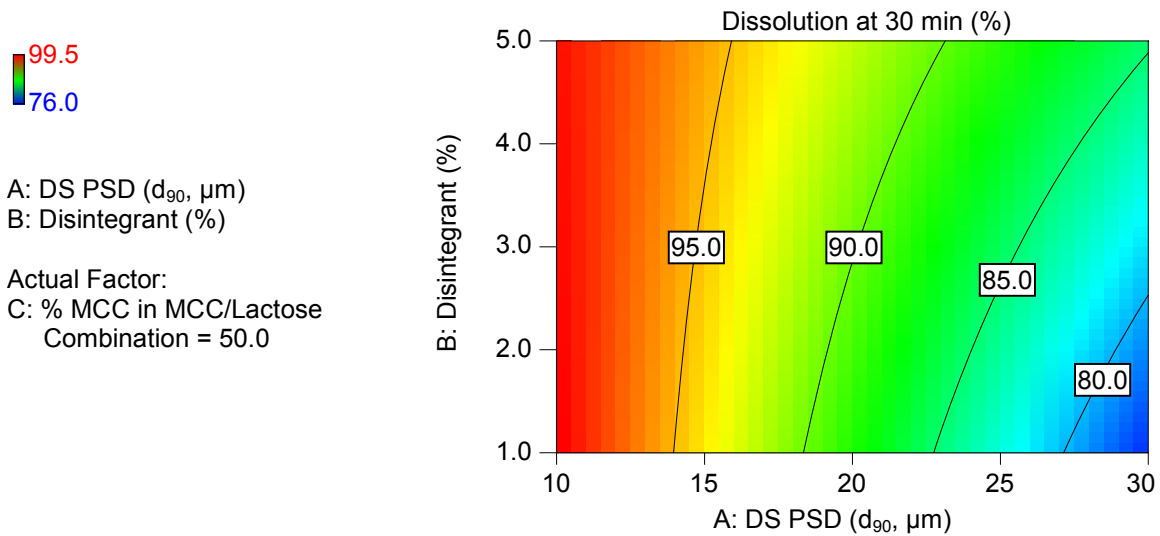


Figure 11. Effect of drug substance PSD and disintegrant level on dissolution at 30 min (tablet target hardness of 12.0 kP)

Significant factors for tablet disintegration time

The disintegrant level was the only statistically significant factor to affect tablet disintegration. However, all batches demonstrated rapid disintegration in less than 4 minutes.

Significant factors for tablet assay

All batches demonstrated acceptable assay (ranging from 98.3-101.2%) which was well within the specification limits (95.0-105.0% w/w) and none of factors showed significant impact on tablet assay.

Significant factors for tablet content uniformity (%RSD)

Data analysis indicated that the curvature effect was not significant for tablet content uniformity. As shown in the half-normal plot (Figure 12), the significant factors affecting tablet content uniformity were A (drug substance PSD) and C (% MCC in the MCC/Lactose combination).

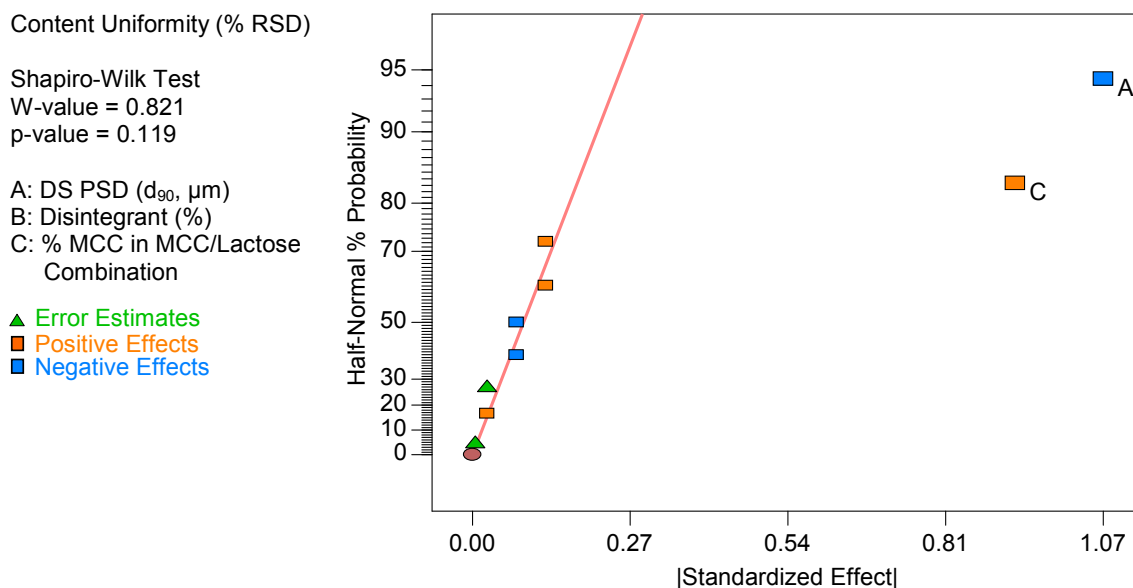


Figure 12. Half-normal plot of the formulation variables effect on tablet content uniformity (% RSD)

Figure 13 shows the effect of drug substance PSD and percentage of MCC in the MCC/Lactose combination on tablet content uniformity. The % RSD decreased with increasing drug substance PSD. On the other hand, % RSD increased with increasing percentage of MCC in the MCC/Lactose combination, likely because the fibrous particle shape of MCC does not flow as well as the spherical particle shape of lactose.

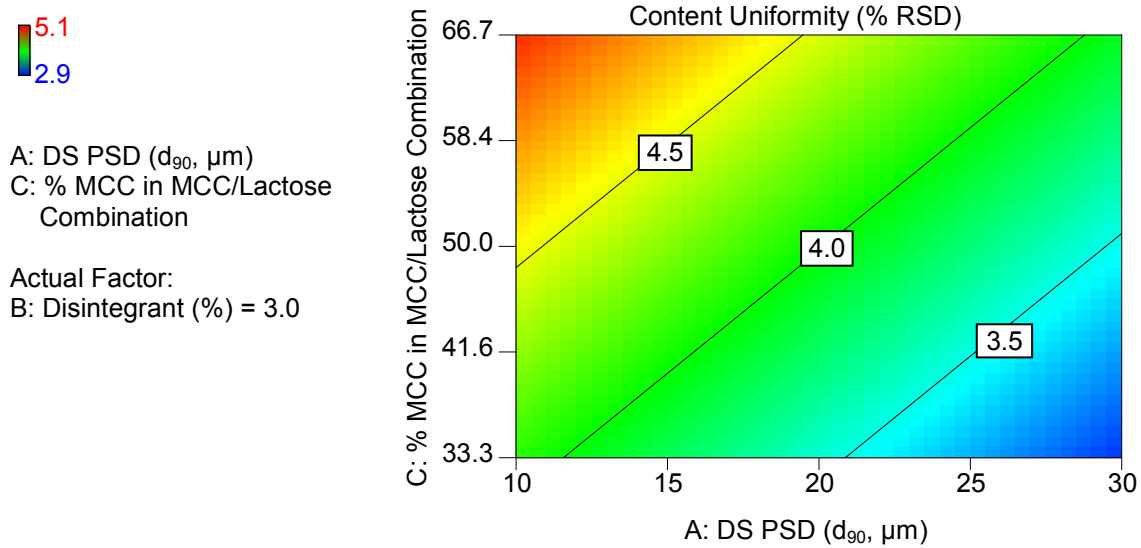


Figure 13. Effect of drug substance PSD and % of MCC in the MCC/Lactose combination on tablet content uniformity (%RSD)

Significant factors for powder blend flowability

The flowability (represented by ffc value) of the powder blend from the pre-roller compaction blending and lubrication step was determined for each sample using a ring shear tester. The ffc of each sample was then recorded. As shown in the half-normal plot (Figure 14), the significant factors affecting powder blend flowability were A (drug substance PSD) and C (% MCC in the MCC/Lactose combination). The effect of drug substance PSD and percentage of MCC in the MCC/Lactose combination on powder blend flowability is shown in Figure 15. Powder blend flowability increased with increasing drug substance PSD and decreasing percentage of MCC in the MCC/Lactose combination.

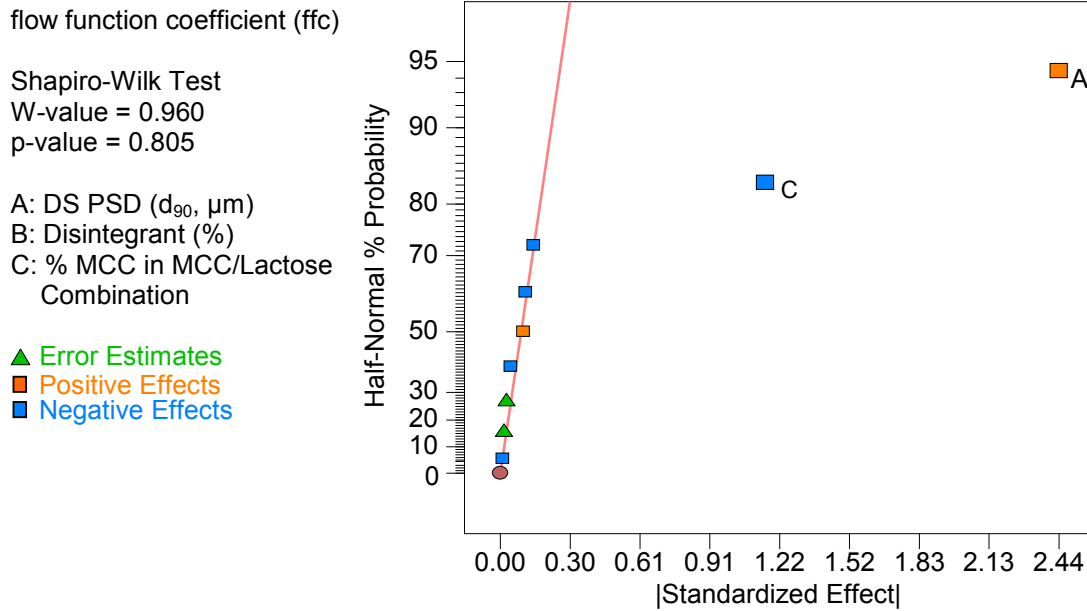


Figure 14. Half-normal plot of the formulation variable effects on powder blend flowability (ffc)

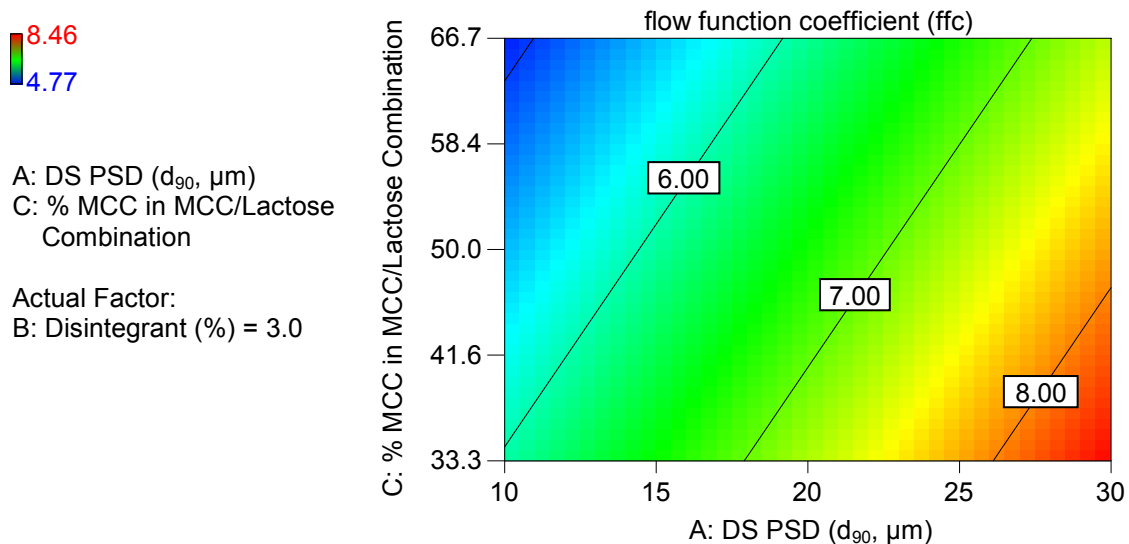


Figure 15. Effect of drug substance PSD and % MCC in the MCC/Lactose combination on flowability (ffc)

Significant factors for tablet hardness

Each DOE batch was compressed at 5 kN, 10 kN and 15 kN to evaluate its tableability. The half-normal plot (Figure 16) shows that the only significant factor affecting tablet hardness when using 10 kN of compression force was C (% MCC in the MCC/lactose combination). A similar relationship was observed for compression forces of 5 kN and 15 kN (*data not shown*). As shown in Figure 17, tablet hardness increased with an increasing percentage of MCC in the MCC/lactose combination at a given compression force.

Hardness @10 kN (kP)

Shapiro-Wilk Test
W-value = 00.914
p-value = 0.465

A: DS PSD (d_{90} , μm)
B: Disintegrant (%)
C: % MCC in MCC/Lactose
Combination

▲ Error Estimates
■ Positive Effects
■ Negative Effects

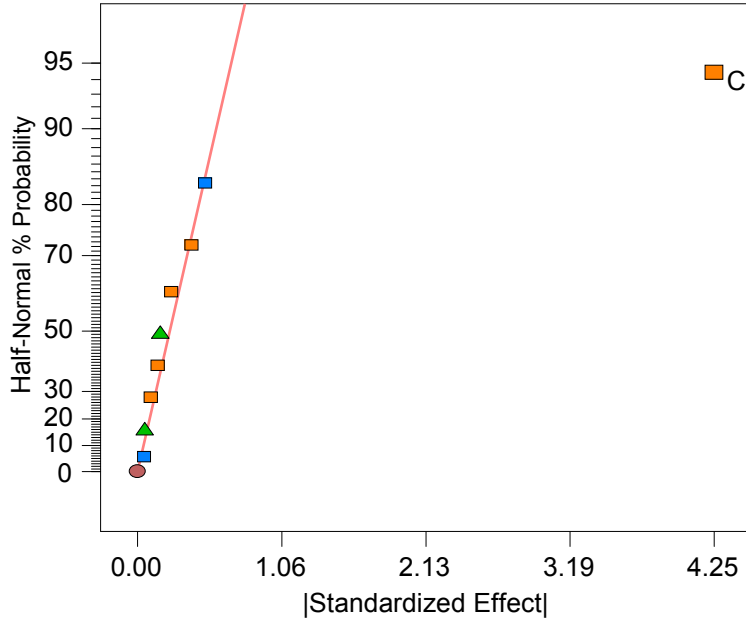


Figure 16. Half -normal plot of the formulation variable effects on tablet hardness @ 10 kN

Hardness @10 kN (kP)

C: % MCC in MCC/Lactose
Combination

Actual Factors:
A: DS PSD (d_{90} , μm) = 20
B: Disintegrant (%) = 3.0

● Design Points

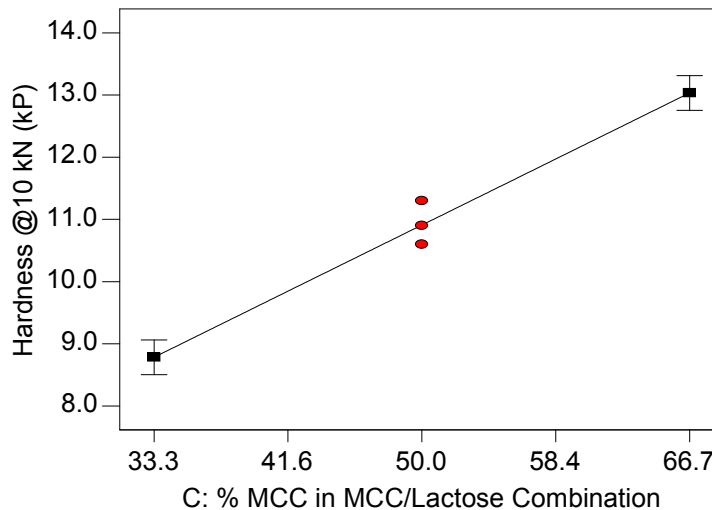


Figure 17. Effect of % MCC in the MCC/Lactose combination on tablet hardness @ 10 kN

Significant factors for tablet friability

All tablets compressed at 5 kN, 10 kN and 15 kN showed good friability (< 0.2% weight loss for a tablet hardness range of 5.0-12.0 kP) and the three formulation variables in the ranges studied did not show any statistically significant impact on tablet friability.

Significant factors for tablet stability (degradation products)

All experimental batches were placed in a stability chamber in an open container for three months at 40 °C/75% RH, and samples were pulled and analyzed periodically. The degradation

product ACE 12345, individual unknown impurities and total impurities were well below the specification limits of 0.5%, 0.2% and 1.0%, respectively. None of the formulation variables showed a statistically significant impact on degradation products.

Summary of Formulation Development Study #1

Acetriptan PSD had a significant impact on tablet dissolution, content uniformity and powder blend flowability. A smaller drug substance PSD enhanced dissolution; however, it negatively impacted tablet content uniformity and blend flowability.

The intragranular disintegrant level showed a significant impact on tablet dissolution due to its interaction with drug substance PSD. The disintegrant level had a greater impact on dissolution when the drug substance PSD was larger.

The percentage of MCC in the MCC/Lactose combination had a significant impact on powder blend flowability, tablet content uniformity and tablet hardness. Increasing the percentage of MCC increased tablet hardness but decreased powder blend flowability and negatively impacted tablet content uniformity as evidenced by the increasing % RSD. To balance blend flowability and tablet hardness, 50% MCC in the MCC/Lactose combination (i.e., 1:1 ratio) was selected for the tentatively finalized formulation.

Because no curvature effects were observed for any of the responses studied, and the main effects and interaction effects were identified using a full factorial DOE with no aliased terms, further studies to optimize the intragranular excipients were unnecessary. The DOE models were used to establish acceptable ranges for formulation variables. Figure 18 shows the overlay plot of all of the responses. The green zone indicates that all of the responses were achieved simultaneously.

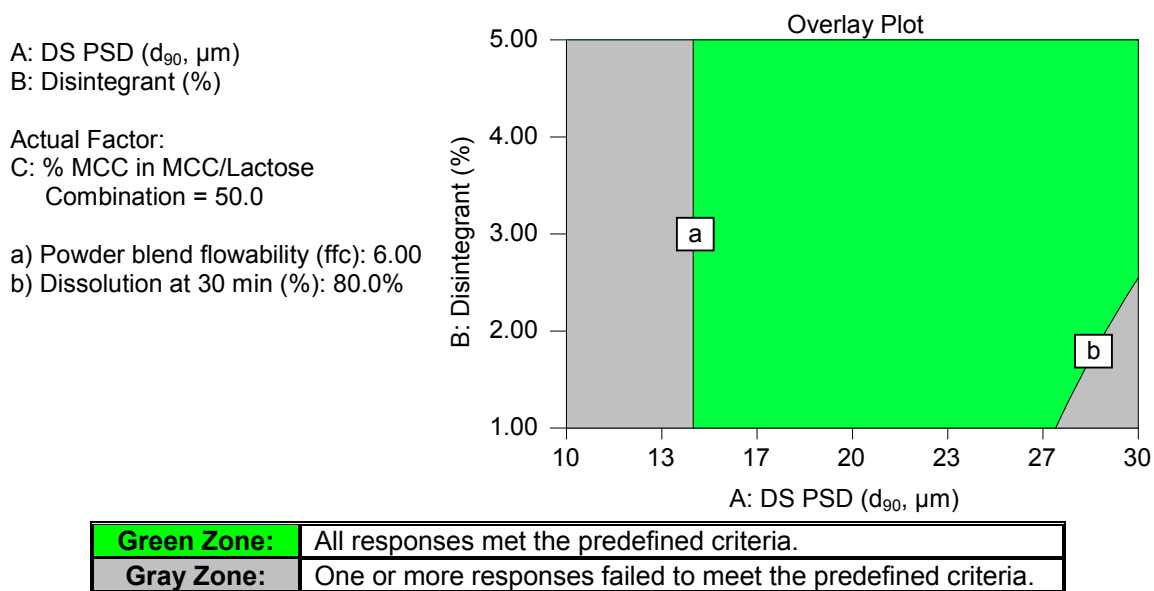


Figure 18. Overlay plot – effect of acetriptan formulation variables on responses

In order to accommodate the largest possible drug substance PSD and to avoid operating on the edge of the green zone where dissolution failure is possible, 5% of croscarmellose sodium was selected for the tentatively finalized formulation. With this selected disintegrant level, the acceptable range for drug substance d_{90} is 14-30 μm . A d_{90} less than 14 μm showed unfavorable flowability resulting in unacceptable tablet content uniformity when the fixed manufacturing process was used during formulation development. Therefore, drug substance PSD was further studied during pre-roller compaction blending and lubrication process development.

In order to understand the impact of drug substance PSD on in vivo performance and to identify the upper particle size limit that was still likely to be bioequivalent, drug substance with a d_{90} of 20 μm , 30 μm and 45 μm (corresponding to d_{50} of 12 μm , 24 μm and 39 μm , respectively) was studied in the pilot BE study (*see Section 1.4*).

At the conclusion of Formulation Development Study #1, the levels of intragranular excipients were tentatively finalized as shown in Table 25. The extragranular glidant and lubricant were further studied in Formulation Development Study #2.

Table 25. Tentative composition of Generic Acetripitan Tablets, 20 mg

Ingredient	Function	Composition	
		(mg/tablet)	(% w/w)
--	--		
Acetripitan	Active	20.0	10.0
Intragranular Excipients			
Lactose Monohydrate, NF	Filler	79.0	39.5
Microcrystalline Cellulose (MCC), NF	Filler	79.0	39.5
Croscarmellose Sodium (CCS), NF	Disintegrant	10.0	5.0
Talc, NF	Glidant/Lubricant	5.0	2.5
Extragranular Excipients			
Magnesium Stearate, NF	Lubricant	2.0	1.0*
Talc, NF	Glidant/Lubricant	5.0	2.5*
Total Weight		200.0	100

*Levels to be studied in Formulation Development Study #2

2.2.1.5 Formulation Development Study #2

Based on the results of Formulation Development Study #1, the intragranular excipients levels were tentatively finalized. However, magnesium stearate was linked to adduct formation with acetripitan during the binary excipient compatibility study (*See Section 2.1.1.2*). The goal of this study was to find the minimum level of extragranular magnesium stearate needed for tableting and to evaluate if an increase in talc could compensate for a reduction in magnesium stearate. The level of extragranular magnesium stearate used in Formulation Development Study #1 was 1.0%. The minimum level recommended in the Handbook of Pharmaceuticals is 0.25%.¹¹ Thus, the extragranular magnesium stearate level was studied between 0.3% and 0.9%. The talc level was adjusted accordingly to maintain a total of 3.5% extragranular glidant and lubricant using a two component mixture DOE.

Table 26 summarizes the mixture component levels and responses studied.

Table 26. Design of the two component mixture DOE to study extragranular magnesium stearate and talc

Extragranular Glidant and Lubricant		Levels		
		-1	0	+1
A	Magnesium stearate (%)	0.3	0.6	0.9
B	Talc (%)	3.2	2.9	2.6
Responses		Goal	Acceptable Ranges	
Y ₁	Tablet appearance	Minimize visual defects	Shiny appearance with smooth surface, no side wall striation	
Y ₂	Tablet tooling appearance	Minimize picking and sticking	Shiny appearance with no evidence of picking or sticking	
Y ₃	Ejection force at 10 kN compression force (N)	Minimize	< 150 N	
Y ₄	Tablet hardness @ 10 kN (kP)	Maximize	> 9.0 kP	
Y ₅	Dissolution at 30 min (%) (with target hardness of 12.0 kP)	Maximize	≥ 80%	
Y ₆	Tablet content uniformity (% RSD)	Minimize % RSD	< 5%	

A 5.0 kg batch of granules was manufactured using the roller compaction process parameters listed in Table 20. The granules were made using the formulation shown in Table 25. The batch of granules was then split into six sub-lots and different amounts of magnesium stearate and talc were added according to the composition shown in Table 27. The final blend was compressed into tablets using 10 kN of force. The experimental results for tablet appearance, tooling appearance, tablet ejection force and hardness at a fixed compression force (10 kN) (Y₁, Y₂, Y₃ and Y₄, other responses not shown) are presented in Table 27.

Table 27. Experimental results of the two component mixture DOE

Batch No.	Mixture Components		Responses			
	Magnesium stearate level	Extragranular talc level	Tablet appearance*	Tooling appearance	Ejection force @10 kN	Tablet hardness @10 kN
	(% w/w)	(% w/w)	--	--	(N)	(kP)
12	0.3	3.2	Poor	Visible indication of sticking on punches and binding in the die	431	12.4
13	0.3	3.2	Poor		448	12.2
14	0.9	2.6	Acceptable	Shiny appearance with no evidence of picking and sticking	91	11.2
15	0.6	2.9	Acceptable		114	12.0
16	0.6	2.9	Acceptable		130	11.6
17	0.9	2.6	Acceptable		100	11.3

*Poor: dull appearance, uneven tablet surface and side wall striation; Acceptable: shiny appearance with smooth surface, no side wall striation

Tablet and tooling appearance

With 0.3% magnesium stearate, significant compression-related issues such as tablet picking, sticking and side wall striation were observed. However, with 0.6% or higher magnesium stearate, tablets were elegant in appearance and showed no evidence of sticking or binding to the tablet tooling.

Ejection force

The ANOVA results provided in Table 28 indicate that the linear mixture components and quadratic term (AB) were significant. Figure 19 shows the effect of the mixture components on ejection force.

Table 28. ANOVA results of the quadratic mixture model

Source	Sum of Squares	df	Mean Square	F Value	p-value	Comments
Model	146563	2	73281.50	702.38	< 0.0001	Significant
Linear Mixture	118336	1	118336.00	1134.21	< 0.0001	Significant
AB	28227	1	28227.00	270.55	0.0005	
Pure Error	313	3	104.33	--	--	--
Total	146876	5	--	--	--	--

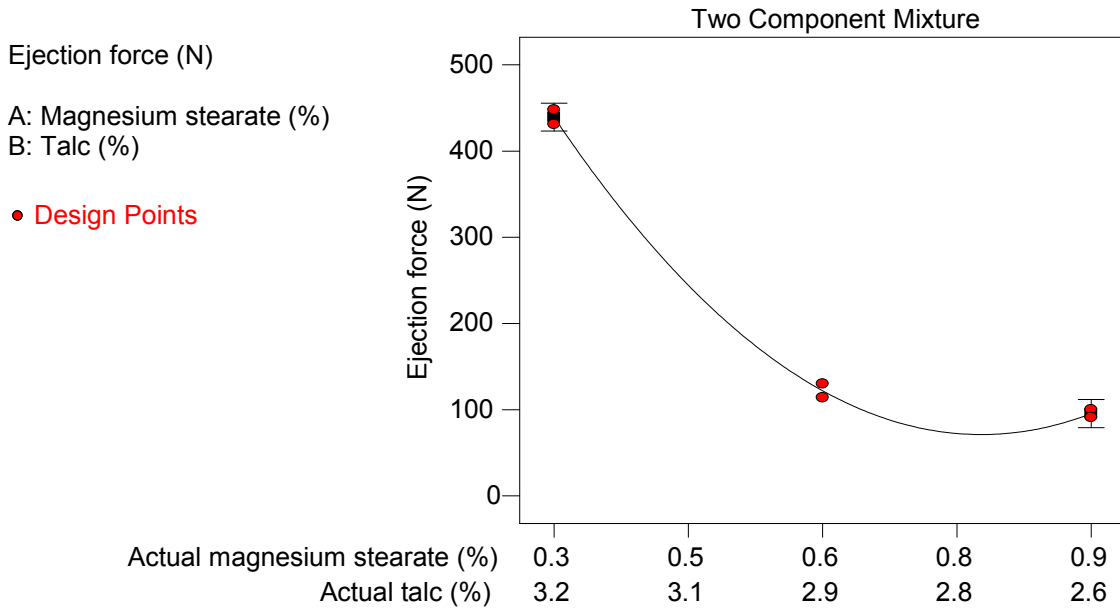


Figure 19. Effect of extragranular magnesium stearate and talc levels on tablet ejection force

With 0.3% magnesium stearate, significantly higher ejection forces were observed. Ejection force decreased with increasing magnesium stearate; however, the impact is negligible once the level is between 0.6%-0.9%.

Tablet Hardness

Figure 20 illustrates the effect of the mixture components on tablet hardness. The tablet hardness observed at a fixed compression force of 10 kN decreased with increasing magnesium stearate.

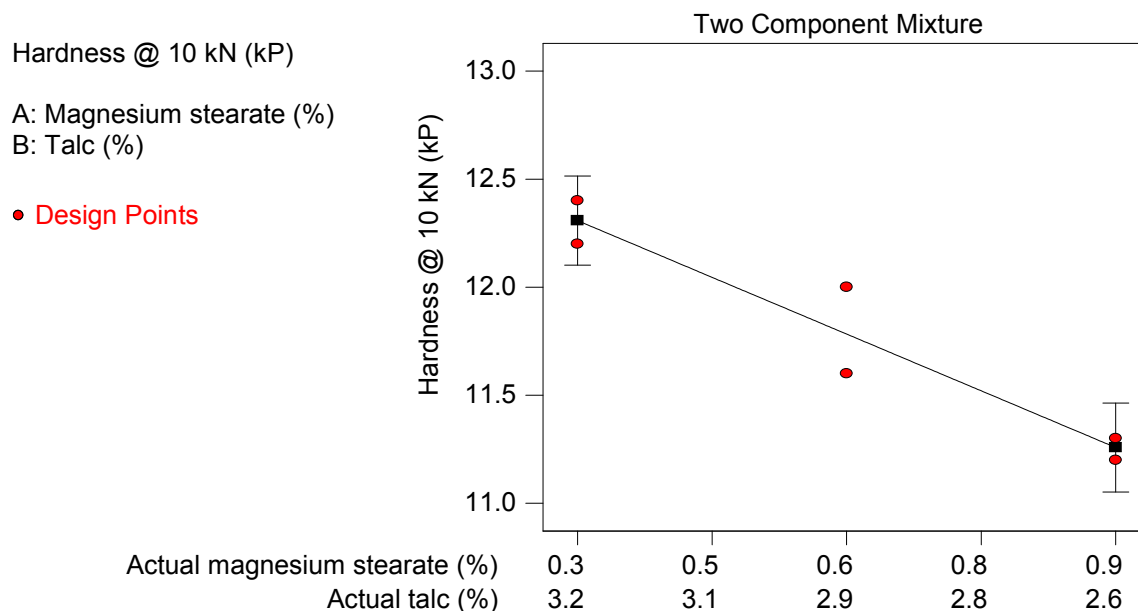


Figure 20. Effect of extragranular magnesium stearate and talc on tablet hardness @ 10 kN

Dissolution and Content Uniformity

All tablets, even those with a hardness of 12.0 kP, exhibited acceptable dissolution (> 85% in 30 min). Content uniformity was not an issue as each batch had a % RSD less than 3%. Therefore, magnesium stearate and talc did not show any significant impact on tablet dissolution and content uniformity within the ranges studied.

Summary of Formulation Development Study #2

Based on the results of Formulation Development Study #2, the extragranular magnesium stearate and talc levels were fixed to 0.6% and 2.9%, respectively.

2.2.1.6 Formulation Development Conclusions

The formulation composition was finalized based on Formulation Development Studies #1 and #2. The MCC/Lactose ratio and the disintegrant level were finalized in the first study. In the second study, it was concluded that a minimum level of magnesium stearate is required in the formulation to prevent picking and sticking. The level of magnesium stearate in the formulation was reduced by using it in combination with talc. The finalized formulation for Generic Acetripitan Tablets, 20 mg, is presented in Table 29.

Table 29. Formulation selected for Generic Acetripitan Tablets, 20 mg¹²

Ingredient	Function	Composition	
		(mg/tablet)	(% w/w)
Acetripitan	Active	20.0	10.0
Intragranular Excipients			
Lactose Monohydrate, NF	Filler	79.0	39.5
Microcrystalline Cellulose (MCC), NF	Filler	79.0	39.5
Croscarmellose Sodium (CCS), NF	Disintegrant	10.0	5.0
Talc, NF	Glidant/Lubricant	5.0	2.5
Extragranular Excipients			
Magnesium Stearate, NF	Lubricant	1.2	0.6
Talc, NF	Glidant/Lubricant	5.8	2.9
Total Weight		200.0	100

2.2.1.7 Updated Risk Assessment of the Formulation Variables

Acceptable ranges for the high risk formulation variables have been established and are included in the control strategy. Based on the results of the formulation development studies, the risk assessment of the formulation variables was updated as given in Table 30 with justifications provided in Table 31.

Table 30. Updated risk assessment of the formulation variables

Drug Product CQAs	Formulation Attributes			
	Drug Substance PSD	MCC/Lactose Ratio	CCS Level	Magnesium Stearate Level
Assay	Low	Low*	Low*	Low*
Content Uniformity	Low	Low	Low*	Low*
Dissolution	Low	Low	Low	Low
Degradation Products	Low*	Low*	Low*	Low

*The level of risk was not reduced from the initial risk assessment.

Table 31. Justification for the reduced risks of the formulation variables

Formulation Variables	Drug Product CQAs	Justification
Drug Substance PSD	Assay	All tablets showed acceptable assay. The risk is reduced from medium to low.
	Content Uniformity	The poor flow of the drug substance is mitigated by using a roller compaction process, low drug load and fillers that have good flowability. The risk is reduced from high to low.
	Dissolution	The risk is reduced from high to low by controlling drug substance PSD and optimizing intragranular superdisintegrant.

¹²All the excipients are present in the RLD.

Formulation Variables	Drug Product CQAs	Justification
MCC/Lactose Ratio	Content Uniformity	The risk is reduced from high to low by optimizing the MCC/Lactose ratio and using a roller compaction process.
	Dissolution	The risk is reduced from medium to low because the selected filler ratio yielded tablets with acceptable friability within a wide range of tablet hardness (5.0-12.0 kP). Tablets with hardness within this range demonstrated acceptable dissolution (> 85% in 30 min).
CCS Level	Dissolution	All tablets showed rapid disintegration. The risk is reduced from high to low.
Magnesium Stearate Level	Dissolution	The risk is reduced from high to low by optimizing extragranular magnesium stearate.
	Degradation Products	The risk is reduced from medium to low by only using magnesium stearate extragranularly and by using talc to minimize the level of magnesium stearate needed. The stability data further demonstrated that the product was stable.

2.2.2 Overages

There are no overages used in the formulation of Generic Acetripitan Tablets, 20 mg.

2.2.3 Physicochemical and Biological Properties

Refer to *Section 1.4* for a discussion of the dissolution method development and the results of the pilot bioequivalence study.

2.3 Manufacturing Process Development

Note to Reader: There are various approaches to process development used in the generic pharmaceutical industry. This is one of many possible examples. All QbD approaches to process development should identify the critical material attributes (CMAs) and critical process parameters (CPPs) for each process step. A firm may choose to do this through reference to documented prior knowledge or through empirical experiments on a range of process scales building toward the exhibit scale and proposed commercial scale. The process development of pre-roller compaction blending and lubrication is an example of experimentally determining CPPs when there is variation in an input material attribute. QbD emphasizes building understanding to avert failures during scale-up. The multivariate experiments described here are a step toward defining acceptable ranges for CPPs and CMAs.

Steps to establish process understanding are as follows:

- *Identify all possible known material attributes and process parameters that could impact the performance of the process.*

- *Use risk assessment and scientific knowledge to identify potentially high risk attributes and/or parameters.*
- *Identify levels or ranges of these potentially high risk attributes and/or parameters.*
- *Design and conduct experiments, using DOE when appropriate.*
- *Analyze the experimental data to determine if a material attribute or process parameter is critical.*
 - *A material attribute or process parameter is critical when a realistic change in that attribute or parameter can significantly impact the quality of the output material.*
- *Develop a control strategy.*

As discussed in *Section 2.2.1.3 Process Selection*, roller compaction was chosen as an appropriate granulation method to avoid drug product degradation and the equipment train was selected. Figure 21 presents the process map for the finalized formulation of Generic Acetripitan Tablets, 20 mg. Each process step in the manufacturing process is listed in the sequence of occurrence. It also presents the material attributes and process parameters that can potentially impact intermediate and finished product quality attributes. The material attributes of the input materials and the process parameters used at the very first process step determine the quality attributes of the output material (intermediate) produced at this step. Material attributes of the intermediate from this step and process parameters of the subsequent process step in the manufacturing process will determine quality attributes of the next intermediate and, eventually, those of the finished drug product. This cycle repeats until the final process step where finished drug product is manufactured and the product quality attributes are evaluated. This map was used to guide the risk assessments performed during process development.

Manufacturing process development studies were conducted at the 5.0 kg lab scale, corresponding to 25,000 units.

Example QbD IR Tablet Module 3 Quality 3.2.P.2 Pharmaceutical Development

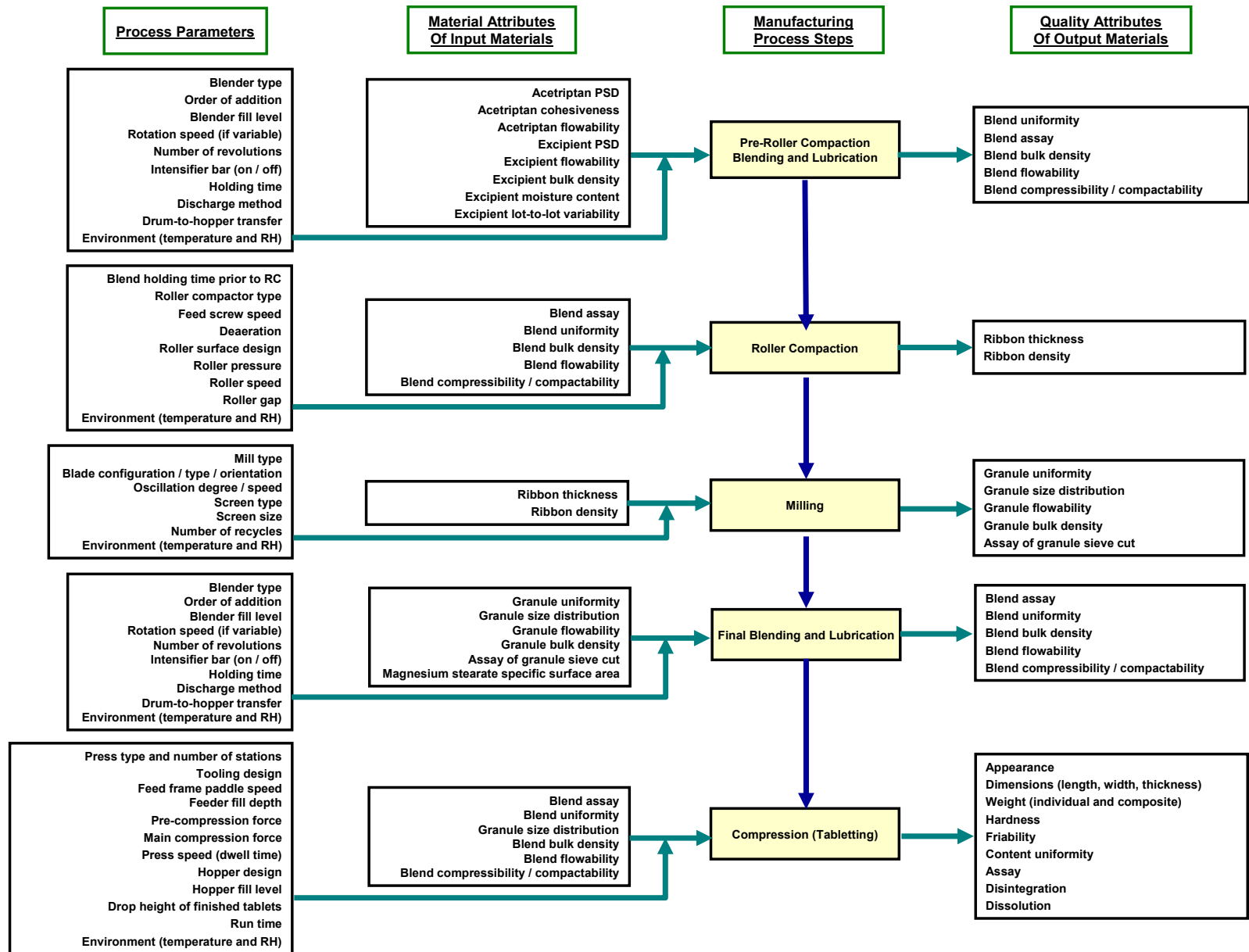


Figure 21. Process map for Generic Acetripitan Tablets, 20 mg

2.3.1 Initial Risk Assessment of the Drug Product Manufacturing Process

A risk assessment of the overall drug product manufacturing process was performed to identify the high risk steps that may affect the CQAs of the final drug product. Subsequently, the intermediate CQAs of the output material from each process step that impact the final drug product CQAs were identified. For each process step, a risk assessment was conducted to identify potentially high risk process variables which could impact the identified intermediate CQAs and, ultimately, the drug product CQAs. These variables were then investigated in order to better understand the manufacturing process and to develop a control strategy to reduce the risk of a failed batch. This method of identifying process variables for further study is illustrated in Figure 22 and is applied in each process step risk assessment.

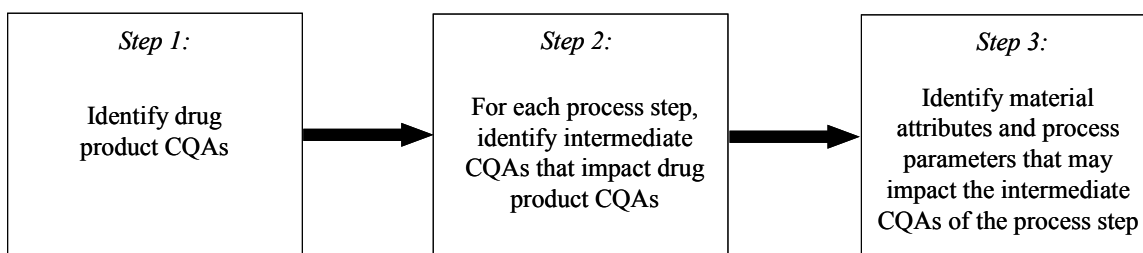


Figure 22. Schematic of the method used to identify process variables for further study

The initial risk assessment of the overall manufacturing process is shown in Table 32 and justifications are provided in Table 33. Previous experience with these process steps was used to determine the degree of risk associated with each process step and its potential to impact the CQAs of the finished drug product.

Table 32. Initial risk assessment of the manufacturing process for Generic Acetripitan Tablets, 20 mg

Drug Product CQAs	Process Steps				
	Pre-RC* Blending and Lubrication	Roller Compaction	Milling	Final Blending and Lubrication	Compression
Assay	Medium	Low	Medium	Low	Medium
Content Uniformity	High	High	High	Low	High
Dissolution	Medium	High	Medium	High	High
Degradation Products	Low	Low	Low	Low	Low

*RC: roller compaction

Table 33. Justification for the initial risk assessment of the manufacturing process for Generic Acetripitan Tablets, 20 mg

Process Steps	Drug Product CQAs	Justification
Pre-Roller Compaction Blending and Lubrication	Assay	Suboptimal pre-roller compaction blending and lubrication may cause variable flowability of the blend. The risk is medium.
	Content Uniformity	The PSD and cohesiveness of the drug substance adversely impact its flowability which, in turn, affects CU. The risk is high.
	Dissolution	Blending process variables may impact the distribution of CCS in the blend which could impact disintegration of the granules and, ultimately, dissolution of the tablets. The risk is medium.
	Degradation Products	Blending process variables are unrelated to the degradation products of Generic Acetripitan Tablets, 20 mg. The risk is low.
Roller Compaction	Assay	Roller compaction is performed to improve flow, minimize segregation and enhance CU. The risk is low.
	Content Uniformity	Variability in ribbon density during processing can potentially impact the PSD of the milled granules, thus impacting flowability and, ultimately, CU. The risk is high.
	Dissolution	Density of the ribbon can impact density and plasticity of the granules, thus impacting compressibility of the granules, hardness of the tablet and, ultimately, dissolution. The risk is high.
	Degradation Products	Based on experience gained from other approved ANDAs using roller compaction, the roller temperature does not exceed 45 °C and the dwell time during roller compaction is very short. Thus, roller compaction should not impact degradation products. The risk is low.
Milling	Assay	The milling step controls the final granule size distribution. A suboptimal distribution may affect flow, causing variable tablet weight and assay during compression. The risk is medium.
	Content Uniformity	If milling generates excessive fines, both bulk density and flowability of the blend may be impacted. This, in turn, may impact CU. The risk is high.
	Dissolution	A large amount of fines may impact tablet hardness and dissolution. The risk is medium.
	Degradation Products	Although the screen may heat up during the milling process, the dwell time is brief. Milling is unlikely to impact degradation products. The risk is low.

Process Steps	Drug Product CQAs	Justification
Final Blending and Lubrication	Assay	The granule uniformity which affects assay and CU is controlled by earlier steps (pre-RC blending and lubrication as well as roller compaction and integrated milling). This step is to blend the granules with small quantities of extragranular glidant and lubricant and is unlikely to impact assay and CU. The risk is low.
	Content Uniformity	
	Dissolution	Over-lubrication due to an excessive number of revolutions may impact disintegration and, ultimately, dissolution of the tablets. The risk is high.
	Degradation Products	Acetripitan is only susceptible to degradation at a high temperature (≥ 105 °C). Blending is unlikely to impact degradation products; therefore, the risk is low.
Compression	Assay	In extreme cases, tablet weight variability can lead to out-of-specification assay results. The risk is medium.
	Content Uniformity	Compression process variables such as feed frame paddle speed and press speed can cause tablet weight variability which could cause tablets to fall out-of-specification for CU. The risk is high.
	Dissolution	Tablet hardness may be impacted if compression force is not adjusted to accommodate batch-to-batch variability in ribbon density. Over-lubrication of the blend by the feed frame paddle may also slow dissolution. The risk is high.
	Degradation Products	Acetripitan is only susceptible to degradation at a high temperature (≥ 105 °C). Compression is unlikely to impact degradation products; therefore, the risk is low.

Further risk assessment was performed subsequently on each high risk process step to identify which process variables may potentially impact the intermediate CQAs. Evaluation of all possible process variables that could potentially impact the quality attributes of the output material of any given process step is not feasible; therefore, some of the variables were set constant based on current understanding.

2.3.2 Pre-Roller Compaction Blending and Lubrication Process Development

Initial Risk Assessment of the Pre-Roller Compaction Blending and Lubrication Process Variables

The initial risk assessment of the overall manufacturing process presented in Table 32 identified the risk of the pre-roller compaction blending and lubrication step to impact tablet content uniformity as high. Subsequently, blend uniformity was identified as an intermediate CQA of the powder blend from the pre-roller compaction blending and lubrication step. Process variables that could potentially impact blend uniformity were identified and their associated risk was evaluated. Table 34 presents the initial risk assessment for the pre-roller compaction blending and lubrication step.

Table 34. Initial risk assessment of the pre-roller compaction blending and lubrication process variables

Process Step: Pre-Roller Compaction Blending and Lubrication		
Output Material CQA: Blend Uniformity		
Variables	Risk Assessment	Justification and Initial Strategy
<i>Input Material Attributes</i>		
Acetriptan PSD	High	The pilot BE study indicated that a $d_{90} \leq 30 \mu\text{m}$ is needed for bioequivalence. Based on several lots of acetriptan analyzed during preformulation, the drug substance meeting this d_{90} criterion has poor flowability ($\text{ffc} < 3.50$) which may impact BU. The risk is high.
Acetriptan cohesiveness	Medium	The specific energy of acetriptan Lot #1-4 indicated that acetriptan is moderately to highly cohesive which will make achieving BU more challenging. The risk is medium.
Acetriptan flowability	Medium	The ffc value of acetriptan Lot #1-4 suggested poor flow which could impact BU. The risk is medium.
Excipient flowability	Low	Filler comprises the majority (~80%) of the formulation. MCC grade B02 and lactose monohydrate grade A01 are used in a 1:1 ratio because this ratio demonstrated good flowability ($\text{ffc} \approx 7$). Glidant and lubricant are used in small quantities and are unlikely to impact BU. The risk is low.
Excipient PSD	Low	Experience with previously approved ANDA 123456 and ANDA 456123 demonstrated that when the selected grades of MCC and lactose monohydrate are used in a 1:1 ratio, the flowability is good. This suggests that the PSD of the fillers will not impact BU. Because the quantities of glidant and lubricant used are small, their PSD are unlikely to impact BU. The risk is low.
Excipient bulk density	Low	The 1:1 ratio of MCC to lactose monohydrate has a comparable bulk density to acetriptan. Glidant and lubricant are used in small quantities and their bulk densities are unlikely to impact BU. The risk is low.
Excipient moisture content	Low	The moisture content of the excipients is controlled per compendial/in-house specifications. Based on previous experience with approved ANDA 123456, excipient moisture content did not exhibit any significant impact on BU. The risk is low.
Excipient lot-to-lot variability	Low	Large variations in the PSD of the excipients could impact BU; however, previous experience with the chosen excipient grades has shown that the lot-to-lot variability within grade is minimal. The risk is low.

Process Step: Pre-Roller Compaction Blending and Lubrication		
Output Material CQA: Blend Uniformity		
Variables	Risk Assessment	Justification and Initial Strategy
Blending Variables		
Blender type	Low	Different blender types have different mixing dynamics. V-blender is selected based on equipment availability. The risk is low. However, if the blender type is changed during scale-up or commercialization, the risk should be re-evaluated.
Order of addition	Low	Order of addition may impact the ease of evenly dispersing ingredients charged in lower quantities. Materials are added in the following order: lactose monohydrate, CCS, acetriptan, talc, and MCC. The risk is low.
Rotation speed (rpm)	Medium	Rotation speed is often fixed by equipment constraint. Different size blenders have different rotation speeds. The rotation speed for the 16 qt blender is fixed at 20 rpm. The risk is medium.
Number of revolutions	High	Under- or over-blending will result in suboptimal BU. The risk is high.
Intensifier bar (on/off)	Low	The intensifier bar is often not needed to improve BU. In addition, the intensifier bar may interfere with BU measurements if an NIR probe is used. The intensifier bar is fixed in the off position. The risk is low.
Blender fill level	High	The blender fill level depends on equipment capacity, blend bulk density (0.43-0.48 g/cc) and batch size. Since the blender fill level may affect mixing dynamics, the risk is high.
Holding time	Medium	Even if adequate BU is achieved, the drug substance may segregate prior to granulation during holding, discharge or transfer. The risk is medium.
Blender discharge	Medium	
Drum-to-hopper transfer	Medium	
Environment (temperature and RH)	Low	If not controlled, fluctuations in the facility temperature and RH could impact BU. Routine environment temperature and RH set point in the cGMP manufacturing facility is fixed at 25 °C ± 5% and 40%-60% RH, respectively, and will be monitored during manufacturing. The risk is low.

Effect of Acetriptan PSD and Number of Revolutions on Blend Uniformity

Due to its low solubility, acetriptan is milled to improve its bioavailability. The milled drug substance has poor flow characteristics and is cohesive. Thus, roller compaction is performed prior to compression to achieve tablet content uniformity. The success of roller compaction to produce uniform granules is largely contingent on the uniformity of the blend achieved during the preceding blending and lubrication step.

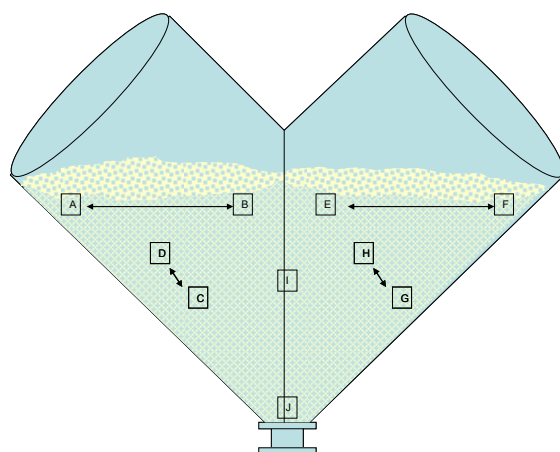
The pilot PK study suggested that Generic Acetriptan Tablets, 20 mg, with a drug substance d_{90} of 30 μm (d_{50} of 24 μm) or less would be bioequivalent to the RLD. During

formulation development, a PSD with a d_{90} less than 14 μm led to flow and content uniformity issues. However, the blending process was fixed at that stage of development. Thus, it was important to determine if an optimized blending process could accommodate different acetyriptan PSD without adversely impacting blend uniformity. A two-factor, three-level full factorial DOE, as shown in Table 35, was used to investigate the impact of acetyriptan PSD (d_{90}) and number of revolutions (N_{rev}) on blend uniformity. Blender fill level is also likely to impact blend uniformity based on the initial risk assessment, but this process parameter was evaluated subsequent to the DOE. The optimized formulation shown in Section 2.2.1.6 Table 29 was used for this study.

Table 35. Design of the 3^2 study to investigate pre-RC blending and lubrication process variables

Factors: Process Variables		Levels		
		0	1	2
A	Number of revolutions (N_{rev})	100	200	300
B	Acetyriptan d_{90} (μm)	10	20	30
Responses		Goal	Acceptable Ranges	
Y_1	Blend Assay (% w/w)	Achieve 100% w/w	Assay mean of all locations: 95.0-105.0% w/w	
Y_2	Blend Uniformity (% RSD)	Minimize % RSD	% RSD of all locations: $\leq 5\%$	

Each 5.0 kg batch was blended in a 16 qt blender operated at 20 rpm. To measure blend uniformity, sampling was performed at the 10 blender locations designated in Figure 23 at the end of the specified number of revolutions. The sample thief was calibrated such that the collected sample volume represented one to three unit doses of blend (200.0-600.0 mg).



- A = Left-Left-Top (left arm)
- B = Left-Right-Top (left arm)
- C = Left-Front-Middle (left arm)
- D = Left-Rear-Middle (left arm)
- E = Right-Right-Top (right arm)
- F = Right-Left-Top (right arm)
- G = Right-Front-Middle (right arm)
- H = Right-Rear-Middle (right arm)
- I = Center-Middle
- J = Discharge Port

Figure 23. Sampling locations in the V-Blender

The blend uniformity results are presented in Table 36.

Table 36. Results of the pre-RC blending and lubrication optimization study

Batch No.	Factors: Process Variables		Response
	A: N _{rev}	B: Acetriptan d ₉₀	Y ₂ : BU
	--	(μm)	(% RSD)
21	100	10	8.9
22	100	30	5.4
23	300	20	2.5
24	100	20	6.8
25	200	20	3.0
26	300	10	3.2
27	300	30	2.3
28	200	30	2.8
29	200	10	4.3

Based on the sum of squares of sequential models (i.e., linear, two factor interaction, quadratic and cubic), the highest order polynomial model was selected where the additional terms were significant and the model was not aliased. The model terms were further reduced based on the significance level ($\alpha = 0.05$) using the backward model selection method.

Significant factors for blend uniformity

The effect of A (N_{rev}) and B (drug substance PSD) on blend uniformity was best described by a quadratic model where the significant factors were A, B, AB interaction and A². The interaction plot below (Figure 24) shows that the blend uniformity response depended on the settings of the two factors. At a lower number of revolutions, the acetriptan PSD had a greater impact on blend uniformity than at a higher number of revolutions. At 100 revolutions, each of the three acetriptan PSD investigated failed to meet the predefined criterion of less than 5% RSD.

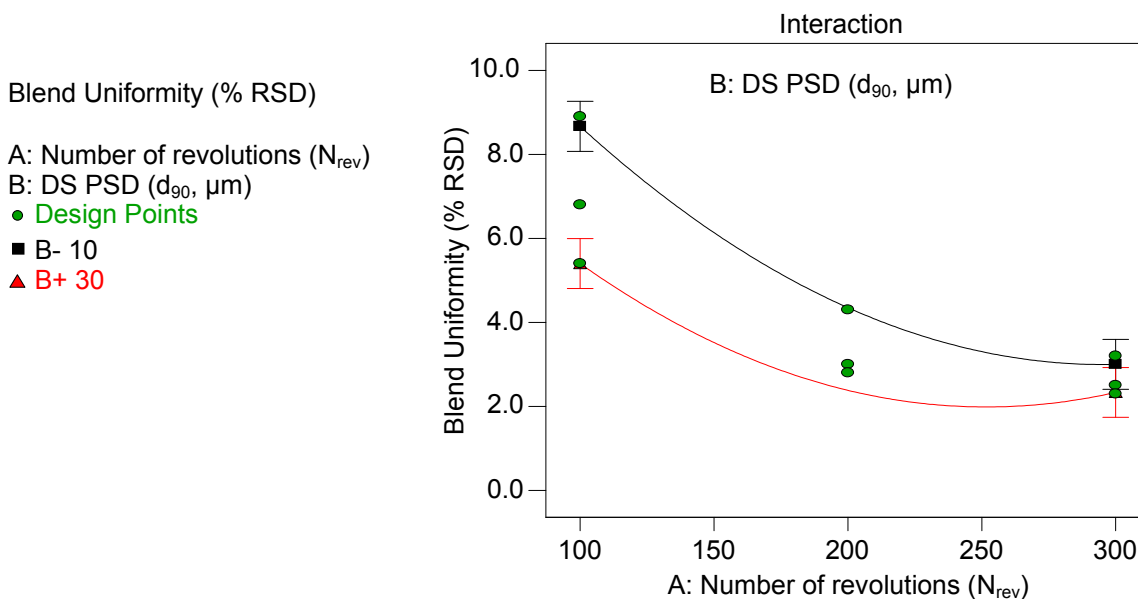


Figure 24. Effect of number of revolutions and drug substance PSD on blend uniformity

Significant factors for blend assay

Neither the number of revolutions nor the drug substance PSD had a significant impact on mean blend assay. Results were close to the target for each run and ranged from 98.7%-101.2% overall.

Development of In-line NIR for Blending Endpoint Determination

Note to Reader: NIR method development and validation is beyond the scope of the pharmaceutical development report and the details are not discussed in this example. The validation report should be included in Section 3.2.P.5.3 Validation of Analytical Procedures.

In order to ensure a homogeneous blend for any input acetriptan drug substance d₉₀ within the range of 10-30 μm, an in-line NIR spectrophotometric method was developed and validated. This technology allows a real-time response and can be used at the laboratory, pilot and commercial scale. During validation, blend uniformity data collected at various time points by the NIR method was compared to that obtained by traditional thief sampling followed by offline HPLC analysis and was found to be comparable. Additionally, validation showed that blends deemed homogeneous by the NIR method ultimately produced tablets with acceptable content uniformity (% RSD < 5%). Based on these findings, the NIR method is capable of accurately assessing the real-time homogeneity of the blend and can be used to control the endpoint of the blending process. Further information regarding the NIR method development and validation can be found in Section 3.2.P.5.3 Validation of Analytical Procedures.

Three 5.0 kg batches (Batch Nos. 30-32) were manufactured using acetriptan with a d₉₀ of 10 μm, 20 μm, and 30 μm, respectively. During blending, one spectrum was acquired

non-invasively through the sight glass of the V-blender for each revolution as the V-blender was in the inverted position. The NIR spectra were preprocessed to minimize the effects of particle size and path length and to resolve the acetriptan peak. To assess the homogeneity of the blend, % RSD was calculated for each moving block of ten consecutive spectra and plotted as a function of number of revolutions. The blend was considered homogeneous once the % RSD was below 5% for ten consecutive measurements. This criterion ensured that brief excursions below the 5% threshold did not result in blending termination.

For an acetriptan d_{90} of 10 μm , 20 μm and 30 μm , the blending endpoint determined by NIR as shown in Figure 25 was 368 revolutions, 285 revolutions and 234 revolutions, respectively. The blending uniformity showed rapid initial change through macro (convection) mixing followed by slower micro (diffusion) mixing.

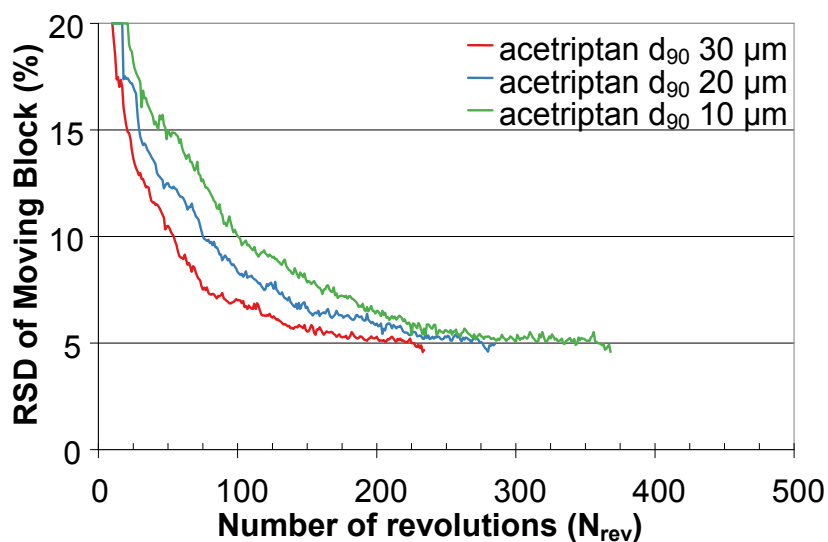


Figure 25. Blending endpoint determined by in-line NIR for acetriptan d_{90} of 10 μm , 20 μm and 30 μm

A fourth 5.0 kg batch (Batch No. 33) was manufactured using acetriptan with a d_{90} of 20 μm . The validated NIR method was used to determine the blending endpoint, but feedback control was not used to terminate the process. Blending was continued for a total of 500 revolutions to look for evidence of demixing. Figure 26 indicates that demixing did not occur as the % RSD did not increase when the batch was blended beyond the NIR-determined endpoint for a total of 500 revolutions.

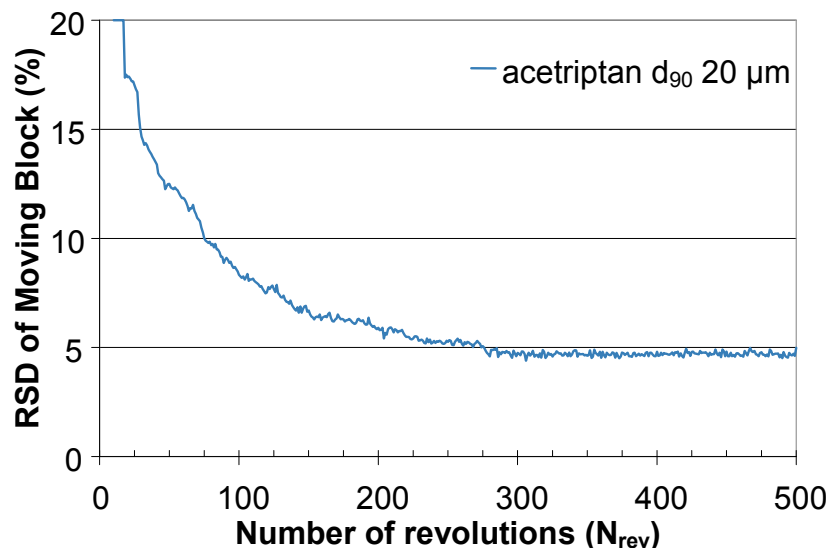


Figure 26. % RSD of the moving block of the NIR spectra for acetriptan d_{90} of 20 μm blended for 500 revolutions

Effect of Blender Fill Level on Blend Uniformity

Another study was performed to evaluate the impact of blender fill level on blend uniformity using acetriptan Lot #2 with a d_{90} of 20 μm . Each blend (Batch Nos. 34-36) was mixed in a 16 qt V-blender at 20 rpm and monitored using an NIR probe. Blend uniformity was achieved at approximately 280-290 revolutions for all three fill levels, 35%, 55% and 75%, indicating that blender fill level does not have a significant impact on the blending endpoint within the range of fill levels studied.

Summary of Pre-Roller Compaction Blending and Lubrication Process Development

Based on the results of the pre-roller compaction blending and lubrication studies, an in-line NIR method will be used to determine the blending endpoint. The number of revolutions needed to achieve blend uniformity differed depending on the acetriptan d_{90} in the range of 10-30 μm . Within the range of 35-75%, the blender fill level did not adversely impact blend uniformity.

Updated Risk Assessment of the Pre-Roller Compaction Blending and Lubrication Process Variables

Table 37 presents the risk reduction for the pre-roller compaction blending and lubrication process as a result of the development studies. Only the process variables that were initially identified as high risk to the blend uniformity are shown.

Table 37. Updated risk assessment of the pre-roller compaction blending and lubrication process variables

Process Step: Pre-Roller Compaction Blending and Lubrication		
Output Material CQA: Blend Uniformity		
Variables	Risk Assessment	Justification for the Reduced Risk
Acetripitan PSD	Low	In order for the blending process to be robust enough to accommodate different acetripitan PSD, an in-line NIR method was developed for blending endpoint determination. Blender fill levels from 35-75% had no impact on blending endpoint. The risk was reduced from high to low.
Number of revolutions	Low	
Blender fill level	Low	

2.3.3 Roller Compaction and Integrated Milling Process Development

Initial Risk Assessment of the Roller Compaction and Integrated Milling Process Variables

Based on the initial risk assessment of the overall manufacturing process shown in Table 32, the risk of the roller compaction step to impact tablet content uniformity and dissolution was identified as high and the risk of the milling step to impact tablet content uniformity was identified as high. Due to equipment availability, an Alexanderwerk¹⁰ WP120 roller compactor with integrated milling was used for this study. Therefore, these two steps were studied together. Subsequently, ribbon density, granule size distribution, granule uniformity and granule flowability were identified as the intermediate CQAs of the output material from the roller compaction and integrated milling step. Ribbon density is an intermediate CQA because it has a direct impact on granule particle size distribution, granule bulk and tapped density, granule flowability, and, ultimately, tablet hardness and dissolution. Granule size distribution, granule uniformity and granule flowability are intermediate CQAs because they are intimately related to tablet weight variability and content uniformity. The input material attributes and process parameters for this step that could potentially impact the four intermediate CQAs of the output material were identified and their associated risk was evaluated. The result of the initial risk assessment is summarized in Table 38.

Table 38. Initial risk assessment of roller compaction and integrated milling process variables

Process Step: Roller Compaction and Integrated Milling			
Output Material CQAs: Ribbon Density, Granule Size Distribution, Granule Uniformity and Granule Flowability			
Variables	Output Material CQAs	Risk Assessment	Justification and Initial Strategy
<i>Input Material Attributes</i>			
Blend bulk density	Ribbon Density	Low	The formulation has been optimized (<i>Section P.2.2</i>). Consistent blend bulk density between 0.43-0.48 g/cc was observed. This low variability of blend bulk density has a negligible impact on the four CQAs. The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Blend assay	Ribbon Density	Low	The assay of the final blend was consistently within 95.0-105.0% w/w (ranging from 98.7-101.2%). The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	

Process Step: Roller Compaction and Integrated Milling			
Output Material CQAs: Ribbon Density, Granule Size Distribution, Granule Uniformity and Granule Flowability			
Variables	Output Material CQAs	Risk Assessment	Justification and Initial Strategy
Blend uniformity	Ribbon Density	Low	In-line NIR monitoring is used to achieve adequate blend uniformity (RSD < 5%). The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Blend compressibility/compactability	Ribbon Density	Low	Compressibility and compactability were optimized during formulation development. The tablet demonstrated good friability (< 0.2% weight loss) at low hardness (5.0 kP) and achieved the desired dissolution at high hardness (12.0 kP). The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Blend flowability	Ribbon Density	Low	The blend demonstrated acceptable flowability (ffc > 6). The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
<i>Roller Compaction and Milling Process Variables</i>			
Pre-RC blend holding time	Ribbon Density	Low	Due to the cohesiveness of acetriptan, no demixing was observed with extended blending up to 500 revolutions. The risk of the pre-RC blend to segregate during holding is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Roller compactor type	Ribbon Density	Low	Due to operating principle differences between roller compactors, the ribbon attributes and PSD of milled granules can vary significantly. Based on availability, Alexanderwerk WP 120 is selected and fixed for development work. The risk is low. However, if the roller compactor type is changed during scale-up or commercialization, the risk should be re-evaluated.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Deaeration	Ribbon Density	Low	Deaeration is used to enhance the flow of the blend feeding into the roller compactor. It will always be used and is considered a fixed factor. The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Feed screw speed	Ribbon Density	Medium	Feed screw speed is a floating parameter dependent on roller pressure and roller gap. The risk is medium.
	Granule Size Distribution	Medium	
	Granule Uniformity	Medium	
	Granule Flowability	Medium	
Roller surface design	Ribbon Density	Low	Roller surface design may impact the power feeding from the slip region into the nip region. For this product, a roller with a knurled surface was selected to enhance material feeding by providing more friction than a smooth surface roller and is considered a fixed factor. The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	

Process Step: Roller Compaction and Integrated Milling			
Output Material CQAs: Ribbon Density, Granule Size Distribution, Granule Uniformity and Granule Flowability			
Variables	Output Material CQAs	Risk Assessment	Justification and Initial Strategy
Roller pressure	Ribbon Density	High	Ribbon density is directly related to roller pressure and, in turn, may impact the PSD, flowability, uniformity, compressibility and compactability of the milled granules. The risk is high.
	Granule Size Distribution	High	
	Granule Uniformity	High	
	Granule Flowability	High	
Roller speed	Ribbon Density	Medium	The roller speed determines the throughput of the process and is adjusted according to the selected feed screw speed to avoid material build-up. In addition, roller speed is inversely related to the dwell time for particle compaction which may impact the ribbon density. Based on previous experience with approved ANDA 123456 using roller compaction, roller speed is fixed to 8 rpm. Adjustment may be needed. The risk is medium.
	Granule Size Distribution	Medium	
	Granule Uniformity	Medium	
	Granule Flowability	Medium	
Roller gap	Ribbon Density	High	According to the Johanson model ¹³ , ribbon density is inversely related to the roller gap and, in turn, it may impact PSD, flowability, uniformity, compressibility and compactability of the milled granules. The risk is high.
	Granule Size Distribution	High	
	Granule Uniformity	High	
	Granule Flowability	High	
Mill type	Ribbon Density	N/A	<i>The ribbon is formed during the roller compaction step.</i>
	Granule Size Distribution	Low	The type of mill governs the type of attrition and impacts the PSD of the milled granules. An integrated mill was selected and is considered a fixed factor. The risk is low.
	Granule Uniformity	Low	
	Granule Flowability	Low	However, if the mill type is changed during scale-up or commercialization, the risk should be re-evaluated.
Mill screen type	Ribbon Density	N/A	<i>The ribbon is formed during the roller compaction step.</i>
	Granule Size Distribution	Low	The mill screen type may impact the granule size distribution, granule uniformity and granule flowability obtained from the milling step. A mesh screen is selected based on availability. The risk is low.
	Granule Uniformity	Low	
	Granule Flowability	Low	If the mill screen type is changed, risk will need to be reassessed.

¹³ Johanson, J. R. A rolling theory for granular solids. ASME, Journal of Applied Mechanics Series E, 1965, 32(4): 842–848.

Process Step: Roller Compaction and Integrated Milling			
Output Material CQAs: Ribbon Density, Granule Size Distribution, Granule Uniformity and Granule Flowability			
Variables	Output Material CQAs	Risk Assessment	Justification and Initial Strategy
Mill speed	Ribbon Density	N/A	<i>The ribbon is formed during the roller compaction step.</i>
	Granule Size Distribution	High	The mill speed may impact the PSD of the milled granules which can potentially impact granule uniformity and flowability. The risk is high.
	Granule Uniformity	High	
	Granule Flowability	High	
Blade configuration	Ribbon Density	N/A	<i>The ribbon is formed during the roller compaction step.</i>
	Granule Size Distribution	Low	The milling blade can apply variable shear to the material based on design. Low shear can result in a coarser but more uniform PSD, whereas high shear can result in a non-uniform, multi-modal PSD. The resulting PSD affects flowability and uniformity. The risk is low because the blade is fixed by equipment design.
	Granule Uniformity	Low	
	Granule Flowability	Low	
Mill screen orifice size	Ribbon Density	N/A	<i>The ribbon is formed during the roller compaction step.</i>
	Granule Size Distribution	High	The mill screen orifice size directly impacts PSD which can potentially impact granule uniformity and flowability. The risk is high.
	Granule Uniformity	High	
	Granule Flowability	High	
Number of recycles	Ribbon Density	Medium	If excessive powder leakage occurs during roller compaction or excessive fines are generated during milling, recycles of the fine particles may be considered. However, the number of recycles may impact the homogeneity of the granule quality attributes. The goal is to not recycle material. The risk is medium.
	Granule Size Distribution	Medium	
	Granule Uniformity	Medium	
	Granule Flowability	Medium	
Environment (temperature and RH)	Ribbon Density	Low	If not controlled, fluctuations in the facility temperature and RH could impact the CQAs. Routine environment temperature and RH set point in the cGMP manufacturing facility is fixed at 25 °C ± 5% and 40%-60% RH, respectively, and will be monitored during manufacturing. The risk is low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	

Effect of Roller Pressure, Roller Gap, Milling Speed and Mill Screen Orifice Size

The main objective of the study was to evaluate the effect of the roller compaction and integrated milling process parameters on the quality attributes of the ribbon, milled granules and finished drug product using DOE. The process parameters investigated were roller pressure, roller gap, milling speed and mill screen orifice size.

A preliminary feasibility experiment was conducted to study the effect of roller pressure on the quantity of by-pass material (un-compacted material). The study showed that

within the roller pressure range of 20-80 bar, the quantity of by-pass material was less than 5% and the potency matched that of the blend fed into the roller compactor. Therefore, the roller pressure range of 20-80 bar was suitable for further studies. During the feasibility study, product temperature was monitored by a non-invasive measuring device. No significant increase (> 5°C) was observed. The ranges for roller gap, mill speed and mill screen orifice size were selected based on previous experience with approved ANDA 123456 and ANDA 456123.

For this study, a 2⁴⁻¹ fractional factorial DOE was used and three center points were included to evaluate if any curvature effects exist. Table 39 presents the study design.

Table 39. Design of the 2⁴⁻¹ DOE to study roller compaction and integrated milling process variables

Defining Relation		I=ABCD		
Resolution		IV		
Factors: Process Variables		Levels		
		-1	0	+1
A	Roller pressure (bar)	20	50	80
B	Roller gap (mm)	1.2	1.8	2.4
C	Mill speed (rpm)	20	60	100
D	Mill screen orifice size (mm)	0.6	1.0	1.4
Responses		Goal		Acceptable Ranges
Y ₁	Ribbon density (g/cc)	Target at 1.1		1.0-1.2
Y ₂	d ₁₀ of milled granules (µm)	Target at 100 µm		50-150 µm
Y ₃	d ₅₀ of milled granules (µm)	Target at 600 µm		400-800 µm
Y ₄	d ₉₀ of milled granules (µm)	Target at 1000 µm		800-1200 µm
Y ₅	Granule uniformity (% RSD)	Minimize % RSD		< 5%
Y ₆	Granule flowability (ffc)	Maximize		> 6
Y ₇	Assay of granule sieve cut (% w/w)	Target at 100% w/w		95.0-105.0% w/w
Y ₈	Tablet hardness @ 5 kN (kP)	Maximize		> 5.0 kP
Y ₉	Tablet hardness @ 10 kN (kP)	Maximize		> 9.0 kP
Y ₁₀	Tablet hardness @ 15 kN (kP)	Maximize		> 12.0 kP
Y ₁₁	Friability @ 5 kN (%)	Minimize		< 1.0%
Y ₁₂	Friability @ 10 kN (%)	Minimize		< 1.0%
Y ₁₃	Friability @ 15 kN (%)	Minimize		< 1.0%
Y ₁₄	Tablet assay (% w/w)	Target at 100% w/w		95.0-105.0% w/w
Y ₁₅	Tablet content uniformity (% RSD)	Minimize % RSD		< 5%
Y ₁₆	Tablet disintegration time (min)	Minimize		< 5 min
Y ₁₇	Dissolution at 30 min (%)	Maximize		> 80%

Approximately 50.0 kg of the intragranular excipients and drug substance (Lot #2) were blended in a 150 L diffusive V-blender operated at 12 rpm. The blender was equipped with an NIR probe to monitor the blending endpoint (RSD < 5%, target revolutions ~234). The powder mixture was subdivided into 11 batches, each ~4.5 kg in size. The remaining 0.5 kg of powder was used as a control and was not roller compacted.

Each batch of blended powder was roller compacted using an Alexanderwerk WP120 (roller diameter 120 mm and roller width 25 mm) using the parameters defined in Table

40. The integrated milling unit on the Alexanderwerk WP120 is equipped with a ribbon crusher and a two-step milling apparatus. The ribbon is crushed into small flakes. The crushed flakes will first go through a coarse screen milling (sizing) step in which the rotor operates at 80% of the milling speed used for the second step. The second step is designed for final milling. In this study, the coarse screen size was fixed at 2.0 mm. The milling speed and milling screen orifice size of the second step are shown in Table 40.

The milled granules were blended with talc for 100 revolutions in a 16 qt V-blender operated at 20 rpm. Magnesium stearate was then added and blended for an additional 80 revolutions. Each batch was compressed into tablets with a target weight of 200.0 mg. The tablet hardness and friability were studied as a function of main compression force. Three compression forces, 5 kN, 10 kN and 15 kN, were used. To study tablet assay, content uniformity (% RSD), disintegration and dissolution, the main compression force was adjusted to achieve a target hardness of 9.0 kP (8.0-10.0 kP was allowed).

Table 40 presents the experimental results for ribbon density, mean granule size (d_{50}), granule flowability (ffc), tablet hardness observed at 10 kN force and tablet content uniformity (% RSD) (*other responses not shown*).

Table 40. Experimental results for the roller compaction and integrated milling DOE

Batch No.	Factors				Responses				
	A: Roller pressure	B: Roller gap	C: Mill speed	D: Mill screen	Y ₁ Ribbon density	Y ₃ Granule d_{50}	Y ₆ Granule Flowability (ffc)	Y ₉ Hardness @ 10 kN	Y ₁₅ Tablet CU
	(bar)	(mm)	(rpm)	(mm)	(g/cc)	(μ m)	--	(kP)	(% RSD)
37	50	1.8	60	1.0	1.132	649	7.64	10.9	3.1
38	20	2.4	100	0.6	0.943	268	4.19	14.4	5.3
39	20	1.2	20	0.6	1.002	264	5.26	13.4	4.2
40	80	2.4	100	1.4	1.211	1227	9.83	10.1	2.1
41	80	1.2	20	1.4	1.285	1257	10.46	7.8	1.4
42	20	2.4	20	1.4	0.942	739	6.28	14.5	3.5
43	50	1.8	60	1.0	1.118	639	7.52	10.7	2.8
44	80	1.2	100	0.6	1.278	346	8.61	9.0	2.7
45	50	1.8	60	1.0	1.104	611	7.88	11.4	2.9
46	20	1.2	100	1.4	1.005	687	7.47	12.9	3.1
47	80	2.4	20	0.6	1.206	328	7.25	10.0	2.8

Significant factors for ribbon density

As shown in the half-normal plot (Figure 27), the significant factors affecting ribbon density were A (roller pressure) and B (roller gap). The effect of roller pressure and roller gap on ribbon density is presented in Figure 28. Ribbon density increased with increasing roller pressure (positive effect) and decreasing roller gap (negative effect).

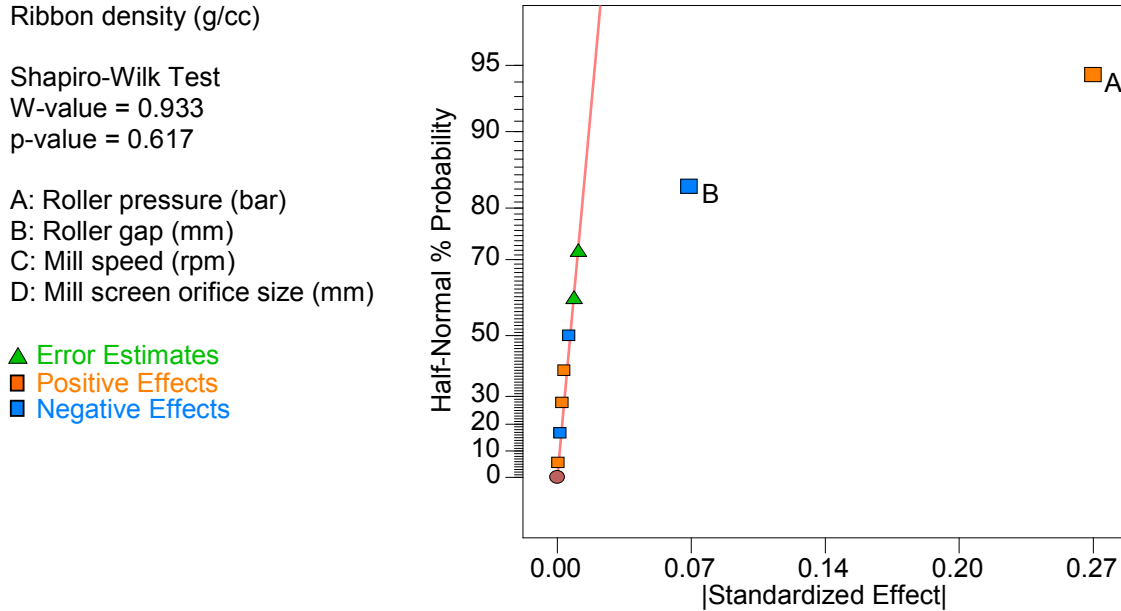


Figure 27. Half-normal plot of the process variable effects on ribbon density

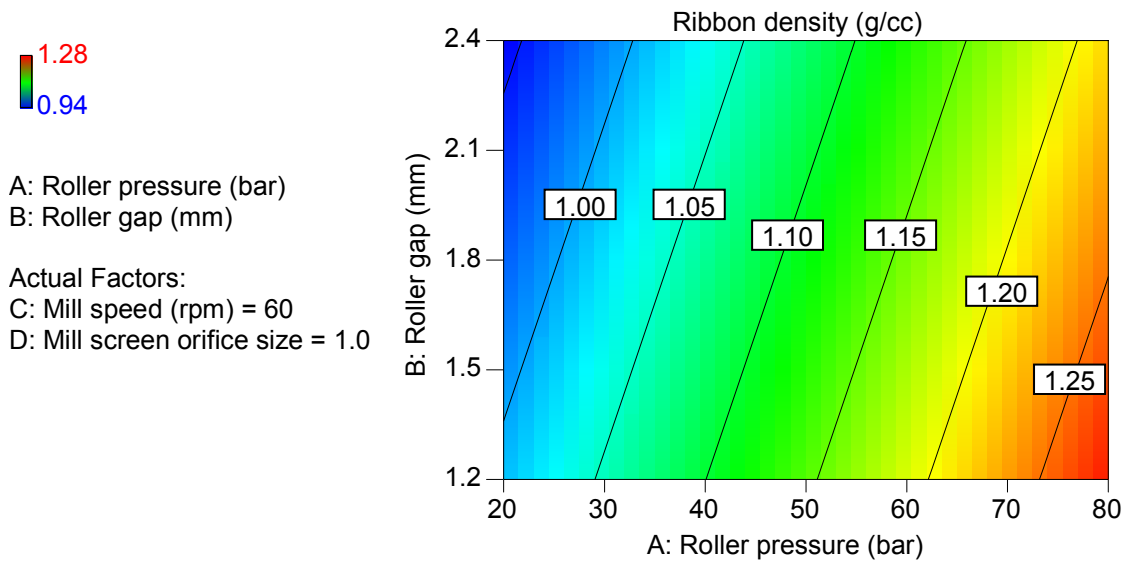


Figure 28. Effect of roller pressure and roller gap on ribbon density

Significant factors for mean granule size (d_{50})

The half-normal plot (Figure 29) shows that the significant factors affecting mean granule size (d_{50}) were D (mill screen orifice size), A (roller pressure) and AD (their interaction).

The contour plot presented in Figure 30 shows the effect of mill screen orifice size and roller pressure on granule d_{50} . It is evident that d_{50} increased with increasing mill screen orifice size and roller pressure (positive effect). These two parameters also exhibited a

strong interaction (i.e., roller pressure showed a larger impact on mean granule size when using a larger mill screen orifice size).

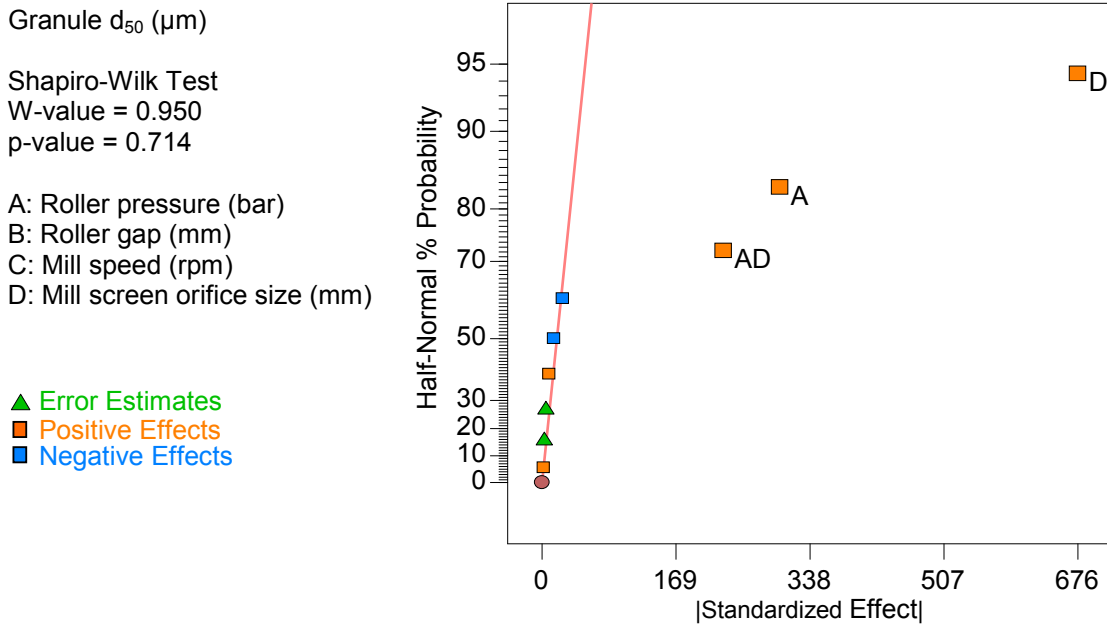


Figure 29. Half-normal plot of the process variable effects on mean granule size (d_{50})

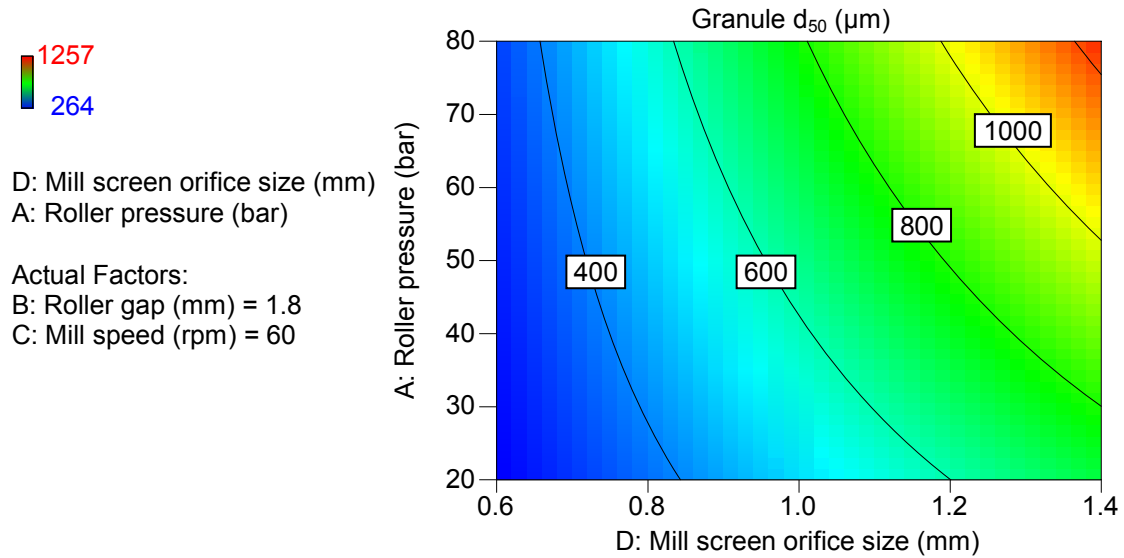


Figure 30. Effect of mill screen orifice size and roller pressure on mean granule size (d_{50})

Significant factors for granule flowability

The flowability (represented by ffc value) of the granules after milling was determined using a ring shear tester. As shown in the half-normal plot (Figure 31), the significant factors affecting granule flowability were A (roller pressure), D (mill screen orifice size) and B (roller gap). The effect of roller pressure and mill screen orifice size on granule flowability is shown in Figure 32. Granule flowability improved with increasing roller pressure and mill screen orifice size. Roller gap also had an impact on granule flowability but to a lesser extent.

Granule flowability (ffc)

Shapiro-Wilk Test
W-value = 0.952
p-value = 0.726

- A: Roller pressure (bar)
- B: Roller gap (mm)
- C: Mill speed (rpm)
- D: Mill screen orifice size (mm)

- ▲ Error Estimates
- Positive Effects
- Negative Effects

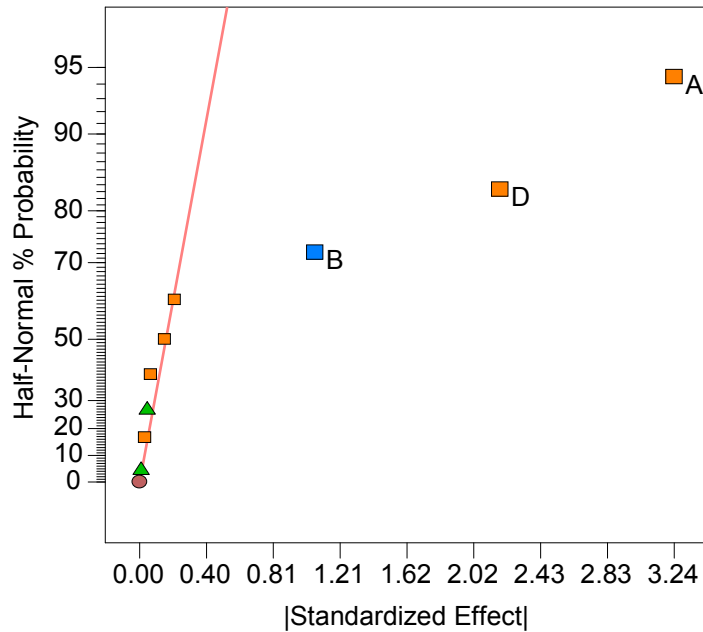


Figure 31. Half-normal plot of the process variable effects on granule flowability (ffc)

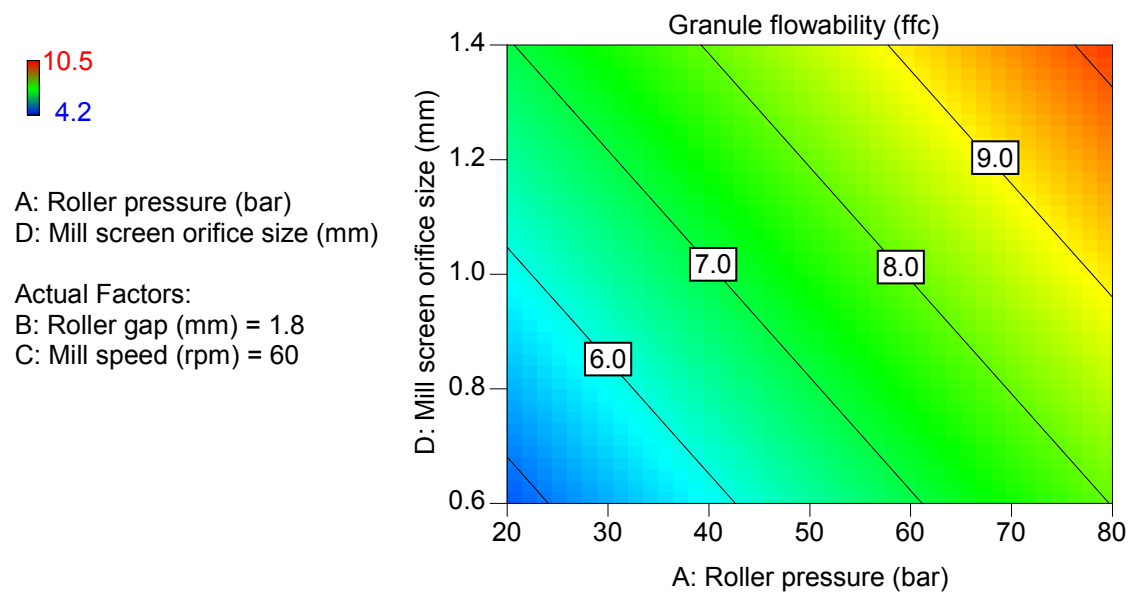


Figure 32. Effect of roller pressure and mill screen orifice size on granule flowability (ffc)

Significant factors for granule uniformity (% RSD)

All batches demonstrated acceptable granule uniformity (ranging from 2.0-2.9% RSD) and none of the process variables showed a significant impact on this response.

Significant factors for assay of granule sieve cuts

Approximately 10 g of granules were sampled from each batch and transferred to the top of a set of seven sieves stacked by decreasing size: 840 µm, 420 µm, 250 µm, 180 µm, 149 µm, 75 µm and pan (no opening for fine collection). The sieves were shaken for five minutes on a laboratory particle size analyzer. The assay of sieve cuts collected from each batch was analyzed. All batches demonstrated acceptable assay for each granule sieve cut (ranging from 98.2-102.0%). This data confirmed that segregation of the pre-roller compacted blend did not occur. None of the factors were shown to have a significant impact on the assay of granule sieve cuts.

Significant factors for tablet hardness

As shown in the half-normal plot (Figure 33), the significant factors affecting tablet hardness when compressed using 10 kN of force were A (roller pressure) and B (roller gap). The effect of roller pressure and roller gap on tablet hardness is presented in Figure 34. Tablet hardness decreased with increasing roller pressure and decreasing roller gap.

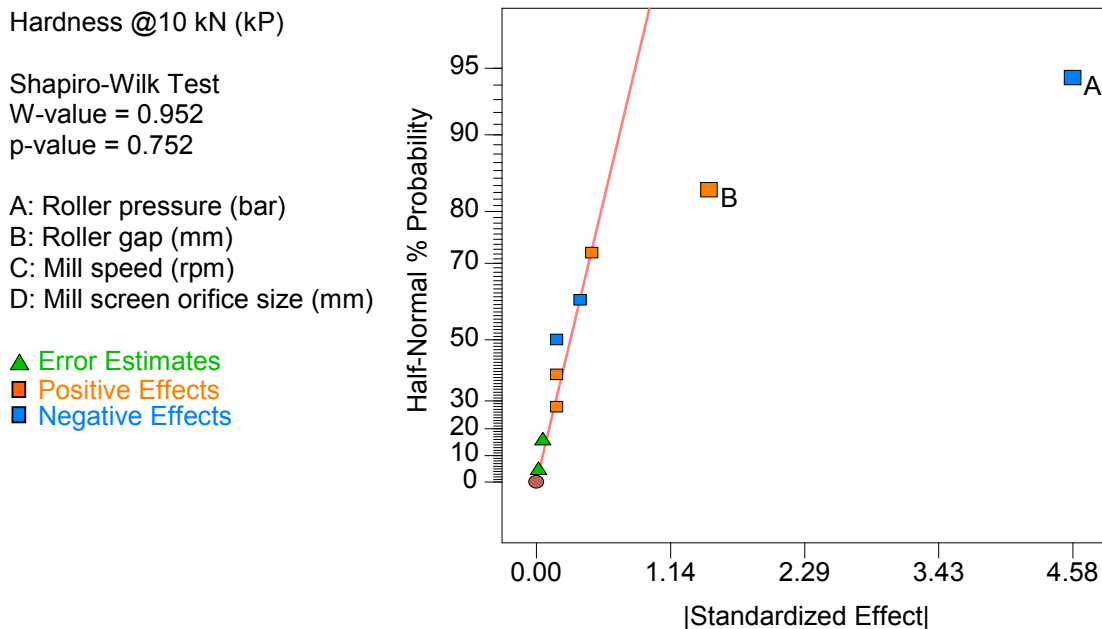


Figure 33. Half-normal plot of the process variable effects on tablet hardness @ 10 kN

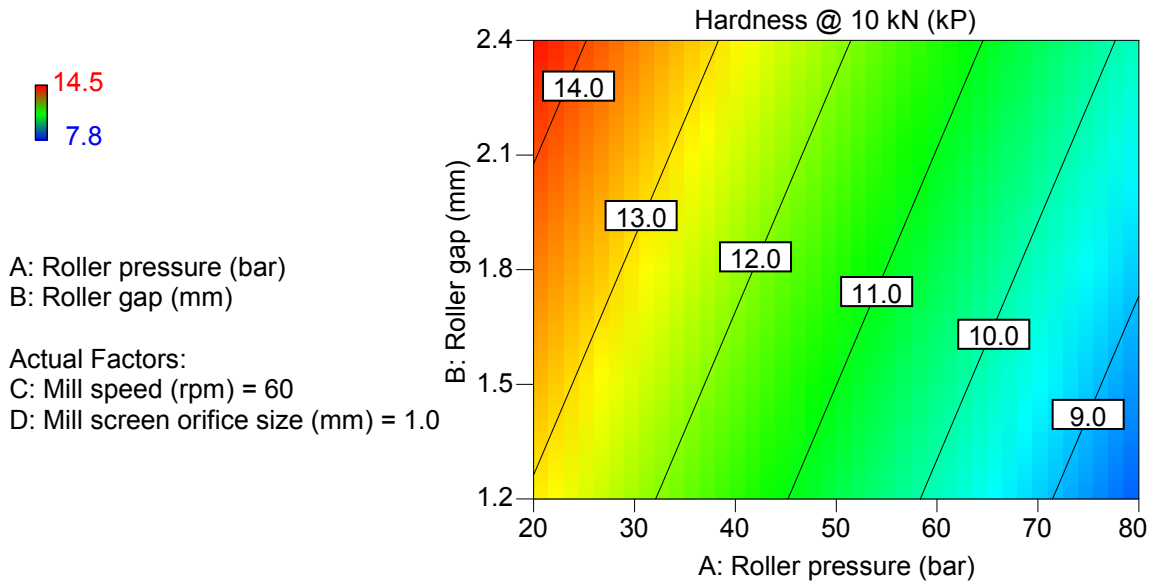


Figure 34. Effect of roller pressure and roller gap on tablet hardness @ 10 kN

Since both ribbon density and tablet hardness were impacted by roller pressure and roller gap, it was logical to evaluate if any correlation existed between these two quality attributes. As shown in Figure 35, an inverse relationship was observed between ribbon density and tablet hardness. The establishment of this relationship was significant as it enables an intermediate material attribute (ribbon density) to be used as an in-process control during roller compaction to facilitate successful downstream operation (tablet compression) and ensure the target for a final product quality attribute (dissolution) is met.

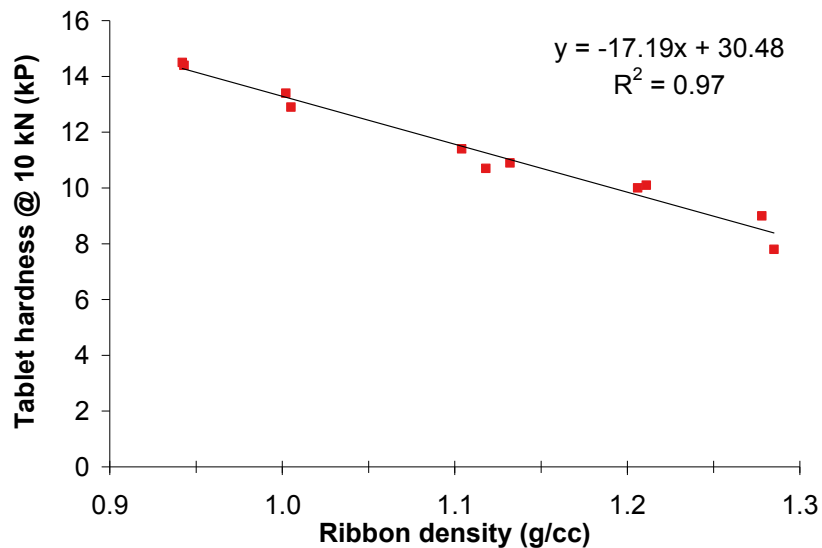


Figure 35. Relationship between ribbon density and tablet hardness

Significant factors for tablet friability

All tablets manufactured in Batch Nos. 37-47 exhibited acceptable friability (< 0.2% weight loss) when compressed using 10 kN and 15 kN of force. When 5 kN of compression force was used, Batch Nos. 41 and 44 exhibited low tablet hardness (< 5.0 kP) and failed the friability test. These two batches had high ribbon density (~ 1.28 g/cc). The remainder of the batches compressed using 5 kN of force showed acceptable friability (< 0.2% weight loss) and hardness was higher than 5.0 kP.

Significant factors for tablet assay

All batches demonstrated acceptable assay (ranging from 98.4-100.6%) which is well within the specification limits (95.0-105.0% w/w) and none of the factors showed a significant impact on tablet assay.

Significant factors for tablet content uniformity (% RSD)

Data analysis indicated that the curvature effect was not significant for tablet content uniformity. As shown in the half-normal plot (Figure 36), the significant factors affecting tablet content uniformity were A (roller pressure), D (mill screen orifice size) and B (roller gap).

Figure 37 shows the effect of roller pressure and mill screen orifice size on tablet content uniformity. Tablet content uniformity improved as evidenced by a decreased % RSD with increasing roller pressure and mill screen orifice size. Roller gap had some impact on tablet content uniformity but to a lesser extent.

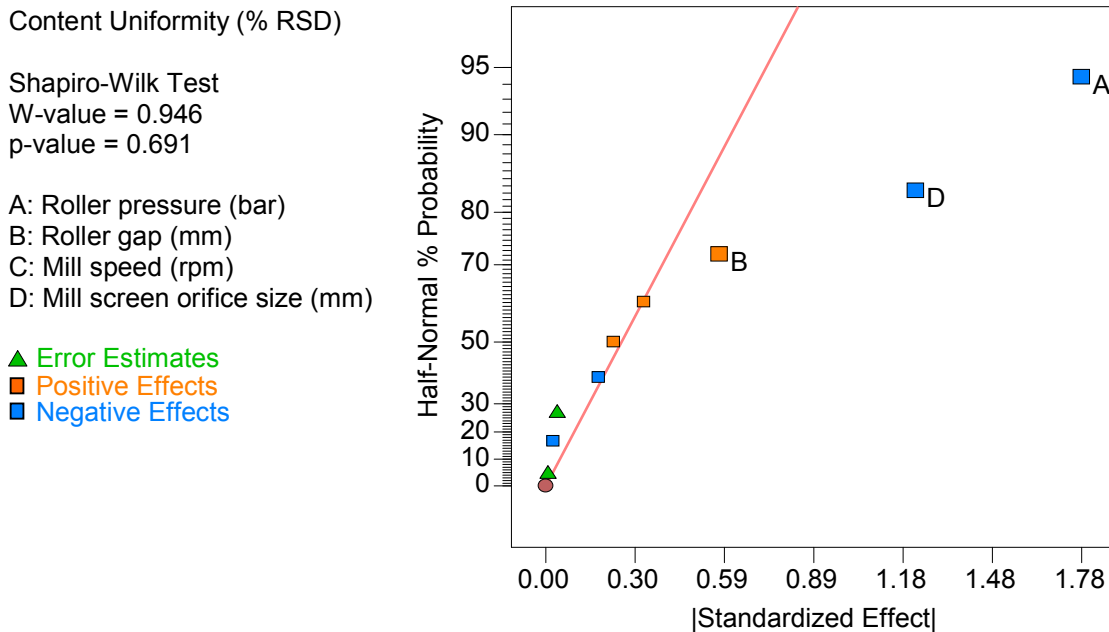


Figure 36. Half-normal plot of the process variable effects on tablet content uniformity (% RSD)

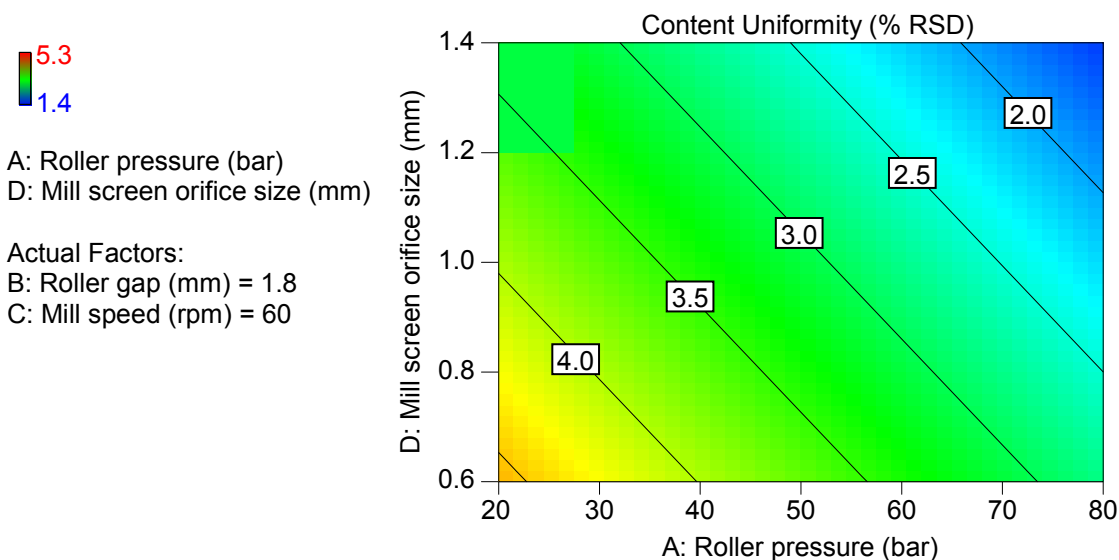


Figure 37. Effect of roller pressure and mill screen orifice size on tablet content uniformity (%RSD)

Significant factors for tablet disintegration

All batches demonstrated rapid disintegration (< 4 min). None of the process variables studied had a significant impact on the disintegration time.

Significant factors for tablet dissolution

Tablet hardness had a significant impact on dissolution (see Section 2.3.5 Tablet Compression Process Development). Based on the inverse linear relationship between ribbon density and tablet hardness, it can be concluded that roller compaction will have an indirect impact on dissolution. For a ribbon with a reasonable density, target hardness can be achieved by adjusting the main compression force. However, it is well known that powder material loses a certain extent of its compressibility and compactability when roller compacted. Consequently, higher compression force is required to achieve the same tablet hardness for a higher ribbon density than for a lower ribbon density. On the other hand, when the ribbon density was low (≤ 1.0 g/cc), the flowability of the granules (Batches 2 and 3) was low ($ffc < 6$). Therefore, a range for ribbon density needs to be established such that the desired granule flowability is achieved and the required compression force will not exceed the maximum allowable tool tip pressure recommended by the tooling manufacturer. Based on the DOE results for tablet friability and granule flowability, the ribbon density will be controlled between 1.0-1.2 g/cc (i.e., ribbon relative density between 0.68-0.81; ribbon true density is 1.4803 g/cc in this study).¹⁴

Summary of roller compaction and integrated milling process development

Roller pressure had a significant impact on ribbon density, mean granule size (d_{50}), granule flowability, tablet hardness and tablet content uniformity. Increasing roller pressure increased ribbon density, granule mean particle size (d_{50}), granule flowability

¹⁴ Ribbon relative density (solid fraction) = ribbon density/ribbon true density.

and tablet content uniformity (lower % RSD). However, it had a negative impact on the compressibility and compactability of the granules as indicated by decreasing tablet hardness for any given compression force.

Roller gap exhibited a significant impact on ribbon density, granule flowability, tablet hardness and tablet content uniformity. Increasing the roller gap decreased ribbon density, granule flowability and tablet content uniformity (higher % RSD). However, tablet hardness at a given compression force increased with increasing roller gap.

Mill screen orifice size had a significant impact on mean granule size (d_{50}), granule flowability and tablet content uniformity. Increasing mill screen orifice size increased granule mean particle size (d_{50}), granule flowability and tablet content uniformity (lower % RSD).

Mill speed did not show a significant impact on any of the responses studied. In addition, no curvature effects were observed for any of the responses. Based on the results of the DOE study, roller pressure, roller gap and mill screen orifice size were identified as the CPPs while mill speed was determined to be not critical.

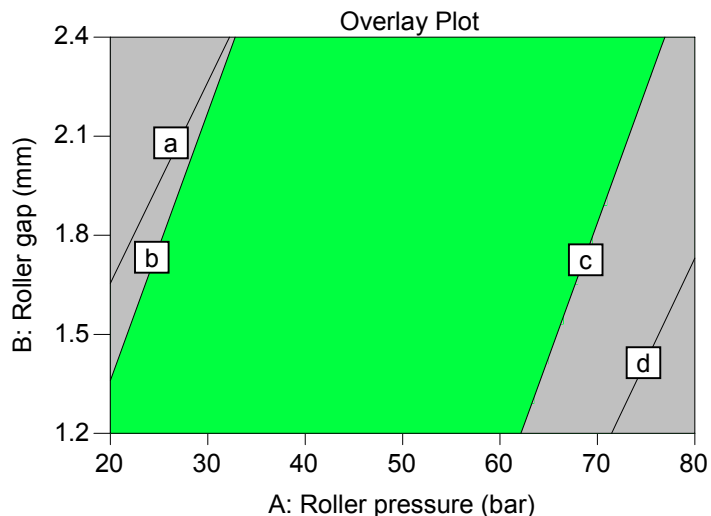
The overlay plot shown in Figure 38 was used to identify an appropriate range for each CPP that would ensure that the targets for all quality attributes are met concurrently. A mill screen orifice size of 1.0 mm was selected because it allows a wider acceptable operating range for both roller pressure and roller gap compared to the other studied sizes (0.6 mm and 1.4 mm). Based on the results, the acceptable ranges for roller pressure and roller gap were identified as 20-77 bar and 1.2-2.4 mm, respectively, for the roller compaction and integrated milling process step using an Alexanderwerk WP120 equipped with a knurled roller that is 120 mm in diameter and 25 mm in width.¹⁵

¹⁵This is for concept demonstration only. All identified CQAs should be studied and included for an actual drug product.

A: Roller pressure (bar)
B: Roller gap (mm)

Actual Factors:
C: Mill speed (rpm) = 60
D: Mill screen orifice size (mm) = 1.0

- a) Granule flowability (ffc): 6.00
- b) Ribbon density (g/cc): 1.000
- c) Ribbon density (g/cc): 1.200
- d) Hardness (kP): 9.0



Green Zone:	All responses met the predefined criteria.
Gray Zone:	One or more responses failed to meet the predefined criteria.

Figure 38. Overlay plot – effect of roller compaction and integrated milling process variables on responses

Updated Risk Assessment of the Roller Compaction and Integrated Milling Process Variables

Table 41 presents the risk reduction for the roller compaction and integrated milling process variables as a result of the development studies. Justification of the reduced risks is also provided.

Table 41. Updated risk assessment of the roller compaction and milling process variables

Process Step: Roller Compaction and Integrated Milling			
Output Material CQAs: Ribbon Density, Granule Size Distribution, Granule Uniformity and Granule Flowability			
Variables	Output Material CQAs:	Risk Assessment	Justification for the Reduced Risks
<i>Roller Compaction and Integrated Milling Process Variables</i>			
Roller pressure	Ribbon Density	Low	An acceptable range for roller pressure was identified during the DOE. Within the range (20-77 bar), all CQAs met the predefined acceptance criteria by using an appropriate roller gap. Thus, the risk is reduced from high to low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Roller gap	Ribbon Density	Low	An acceptable range for roller gap was identified during the DOE. Within the range (1.2-2.4 mm), all CQAs met the predefined acceptance criteria by using an appropriate roller pressure. Thus, the risk is reduced from high to low.
	Granule Size Distribution	Low	
	Granule Uniformity	Low	
	Granule Flowability	Low	
Mill speed	Granule Size Distribution	Low	The mill speed range investigated (20-100 rpm) had no impact on granule PSD, granule uniformity or granule flowability. Thus, the risk is reduced from high to low.
	Granule Uniformity	Low	
	Granule Flowability	Low	

Process Step: Roller Compaction and Integrated Milling			
Output Material CQAs: Ribbon Density, Granule Size Distribution, Granule Uniformity and Granule Flowability			
Variables	Output Material CQAs:	Risk Assessment	Justification for the Reduced Risks
Mill screen orifice size	Granule Size Distribution	Low	The mill screen orifice size (1.0 mm) was selected because it allows a wider acceptable operating range for both roller pressure and roller gap compared to the other studied sizes (0.6 mm and 1.4 mm). When using the selected mill screen orifice size (1.0 mm), all CQAs met the predefined acceptance criteria. Thus, the risk is reduced from high to low.
	Granule Uniformity	Low	
	Granule Flowability	Low	

2.3.4 Final Blending and Lubrication Process Development

Initial Risk Assessment of the Final Blending and Lubrication Process Variables

The initial risk assessment of the overall manufacturing process presented in Table 32 identified the risk of the final blending and lubrication step to impact tablet dissolution as high. The lubrication process variables that could potentially impact tablet dissolution were identified and their associated risk was evaluated. Table 42 presents the initial risk assessment of the final blending and lubrication step.

Table 42. Initial risk assessment of the final blending and lubrication

Process Step: Final Blending and Lubrication		
Output Material CQA: Tablet Dissolution		
Variables	Risk Assessment	Justification and Initial Strategy
<i>Input Material Attributes</i>		
Granule uniformity	Low	The granules produced during roller compaction development demonstrated uniformity with % RSD < 3%. Therefore, granule uniformity should have little impact on tablet dissolution. The risk is low.
Assay of granule sieve cut	Low	Sieve cuts studied during roller compaction development ranged in assay from 98.2% to 101.2%. This low variability will have little impact on tablet dissolution. The risk is low.
Granule flowability	Low	For a ribbon relative density of 0.68 to 0.81, the flowability was good (ffc > 6) and should not impact tablet dissolution. The risk is low.
Granule size distribution	Low	The rapid disintegration of the tablets is achieved by using 5% CCS in the formulation. The variability in granule size distribution observed during roller compaction development showed no impact on dissolution. Therefore, the risk is low.
Granule bulk density	Low	The granule bulk density is consistently between 0.62-0.69 g/cc. The low variability has little impact on tablet dissolution. The risk is low.

Process Step: Final Blending and Lubrication		
Output Material CQA: Tablet Dissolution		
Variables	Risk Assessment	Justification and Initial Strategy
Magnesium Stearate specific surface area	High	The lubricating effect of magnesium stearate improves as specific surface area increases. The risk of over-lubrication leading to retarded disintegration and dissolution is high.
<i>Lubrication Variables</i>		
Blender type	Low	Due to differences in the operating principle, different types of blenders may impact blending efficiency. Based on availability, V-blender is selected. The risk is low. However, if the blender type is changed during scale-up or commercialization, the risk should be re-evaluated.
Order of addition	Low	Granules and talc are blended together first, followed by magnesium stearate. Magnesium stearate is traditionally charged last to lubricate the other particles. Order of addition is fixed and has a minimal impact on dissolution. The risk is low.
Rotation speed (rpm)	Medium	Rotation speed is often fixed by equipment constraint. Different size blenders have different rotation speeds. The rotation speed for the 16 qt blender is fixed at 20 rpm. The risk to impact tablet dissolution is medium.
Number of revolutions	High	Over-lubricating may result in retarded disintegration and dissolution. For a BCS class II compound like acetriptan, the risk is high.
Intensifier bar (on/off)	Low	If the intensifier bar is on, then it may cause granule attrition. To avoid generating fines, the intensifier bar is fixed in the off position during the final blending and lubrication. The risk is low.
Blender fill level	Medium	Blender fill level may affect mixing dynamics. It is fixed for these development studies but could change upon scale-up. The risk is medium.
Holding time	Low	These three process variables are not related to dissolution. The risk is low.
Blender discharge	Low	
Drum-to-hopper transfer	Low	
Environment (temperature and RH)	Low	If not controlled, fluctuations in the facility temperature and RH could impact the CQAs. Routine environment temperature and RH set point in the cGMP manufacturing facility is fixed at 25 °C ± 5% and 40%-60% RH, respectively, and will be monitored during manufacturing. The risk is low.

Based on the results of Formulation Development Study #2, the extragranular magnesium stearate and talc levels were fixed to 0.6% and 2.9%, respectively. The composition of Generic Acetriptan Tablets, 20 mg, was shown previously in Table 29.

Due to the low solubility of acetriptan, it is important to ensure that the blend is not over-lubricated, leading to retarded disintegration. NIR monitoring of the lubrication process is not feasible due to the low amount of lubricant added; therefore, a traditional method with the blending endpoint based on lubrication time is needed.

A study was performed to investigate the effect of magnesium stearate specific surface area and number of revolutions during lubrication on tablet hardness, disintegration, and dissolution. For this study, a 25.0 kg blend was manufactured in a pilot scale blender (150 L) using acetriptan Lot #2. The blend was roller compacted to give a ribbon relative density of 0.75. The ribbon was then milled and subdivided into five 5.0 kg batches. For each batch, the granules and talc were blended for 100 revolutions in a 16 qt V-blender at 20 rpm prior to lubrication with magnesium stearate. Then, magnesium stearate was added and blended according to the experimental design as shown in Table 43. After lubrication, samples were pulled from the 10 locations shown in Figure 23 to verify blend uniformity. The lubricated blend was then compressed using 10 kN of force to manufacture tablets. Ejection force was monitored. Compressed tablets were checked for appearance and the tablet press tooling (punches and dies) was evaluated for evidence of picking/sticking and binding. Additionally, tablets were subjected to friability, assay and content uniformity testing. Table 43 shows the lubrication parameters and results for each batch (*not all data shown*).

Table 43. Results of the extragranular lubrication study*

Batch No.	Factors: Process Variables		Responses			
	A: Magnesium stearate specific surface area	B: N _{rev} (lubrication time)	Y ₁ : BU	Y ₂ : Hardness	Y ₃ : Disintegration time	Y ₄ : Dissolution at 30 min
	(m ² /g)	--	(% RSD)	(kP)	(min)	(%)
48	5.8	60 (3 min)	2.3	9.0	2.7	96.2
49	5.8	100 (5 min)	2.5	9.2	3.1	97.4
50	10.4	60 (3 min)	2.4	8.9	3.4	96.3
51	10.4	100 (5 min)	2.3	8.8	3.7	96.7
52	8.2	80 (4 min)	2.4	9.1	2.9	97.1

*The fill level is ~ 49% and the headspace fraction is ~51%

The ejection force increased slightly with decreased lubrication time and lower specific surface area but did not exceed 150 N during the study. Tablet elegance was not an issue as all compressed tablets had a smooth surface and lacked any visible striations on the sides of the tablet. There was no evidence of product sticking on the punches within the letters and numbers. There was also no evidence of binding to the die cavities.

For each batch, the % RSD was less than 3% indicating that blend uniformity was acceptable following lubrication of the granules. Overall, the blend assay was between 98.3% and 101.7% for all samples pulled during the study. The tablet hardness observed was 9.0 ± 0.2 kP which is well within the target range of 8.0-10.0 kP. Tablets exhibited rapid disintegration (< 4 min) and dissolution (> 95% in 30 min). The results indicated that adequate lubrication of the granules was insensitive to both specific surface area (5.8-10.4 m²/g) and lubrication time (3-5 min) within the ranges studied.

Over the course of the study, friability did not exceed 0.2% w/w. Tablet assay was close to target and well within the acceptable range of 95.0-105.0% w/w. Tablet content uniformity was acceptable with a % RSD less than 4%.

Summary of Final Blending and Lubrication Process Development

Within the ranges studied, magnesium stearate specific surface area (5.8-10.4 m²/g) and number of revolutions (60-100) did not have a significant impact on the drug product quality attributes studied.

Updated Risk Assessment of the Final Blending and Lubrication Process Variables

Table 44 presents the risk reduction for the final blending and lubrication step as a result of the development studies. Only the process variables that were initially identified as high risk to the dissolution of the final drug product are shown.

Table 44. Updated risk assessment of the final blending and lubrication process variables

Process Step: Final Blending and Lubrication		
Output Material CQA: Tablet Dissolution		
Variables	Risk Assessment	Justification for the Reduced Risks
Magnesium stearate specific surface area	Low	Within the range 5.8-10.4 m ² /g, magnesium stearate specific surface area does not adversely impact tablet dissolution. The risk is reduced from high to low and this material attribute will be controlled in the control strategy.
Number of revolutions	Low	A proven acceptable range for number of revolutions (60-100) was established for this scale based on elegant tablet appearance and rapid dissolution. The risk is reduced from high to low and number of revolutions is controlled in the control strategy.

2.3.5 Tablet Compression Process Development

Initial Risk Assessment of the Tablet Compression Process Variables

Based on the initial risk assessment of the overall manufacturing process shown in Table 32, the risk of the compression step to impact content uniformity and dissolution of the tablets was identified as high. Process variables that could potentially impact these two drug product CQAs were identified and their associated risk was evaluated. The results of the initial risk assessment of the compression process variables are summarized in Table 45.

Table 45. Initial risk assessment of the tablet compression process variables

Process Step: Tablet Compression			
Drug Product CQAs: Content Uniformity, Dissolution			
Variables	Drug Product CQAs	Risk Assessment	Justification and Initial Strategy
Input Material Attributes			
Blend assay	Content Uniformity	Low	The blend assay varied between 98.3% and 101.7% during the lubrication process development. This low variability is unlikely to impact CU and dissolution. The risk is low.
	Dissolution	Low	
Blend uniformity	Content Uniformity	Low	The lubricated blend demonstrated acceptable BU (% RSD < 3%) during the lubrication process development. Therefore, the risk is low.
	Dissolution	Low	
Granule size distribution	Content Uniformity	Low	The granule size distribution is controlled by milling after the roller compaction process step. The granules demonstrated good flowability (ffc > 6) and should not impact CU. The risk is low.
	Dissolution	Low	The formulation contains 5% CCS and the variability in granule size distribution observed during roller compaction development showed no impact on dissolution. The risk is low.
Blend flowability	Content Uniformity	Low	Blend flowability could impact powder flow from the hopper to the feed frame and, ultimately, to the die cavity. However, adequate flow was demonstrated during roller compaction development. Small amounts of extragranular glidant and lubricant will not impact blend flowability. The risk is low.
	Dissolution	Low	
Blend compressibility and compactability	Content Uniformity	Low	CU is unaffected by the blend compressibility and compactability. The risk is low.
	Dissolution	High	Suboptimal blend compressibility and compactability can affect tablet hardness. The compressibility and compactability of the blend are directly related to the ribbon relative density achieved during roller compaction. Ribbon relative density may vary from batch-to-batch and may cause tablet hardness variation if the compression force is not adjusted. This may, in turn, impact dissolution. The risk is high.
Blend bulk density	Content Uniformity	Low	The blend bulk density is consistently between 0.62-0.69 g/cc. The low variability has little impact on CU and dissolution. The risk is low.
	Dissolution	Low	
Compression Variables			
Press type and number of stations used	Content Uniformity	Low	The press type was selected based on equipment availability and 3 stations will be used during development. The same press model but all 51 stations will be used for both exhibit and commercial scale. Thus, the risk is low.
	Dissolution	Low	

Process Step: Tablet Compression			
Drug Product CQAs: Content Uniformity, Dissolution			
Variables	Drug Product CQAs	Risk Assessment	Justification and Initial Strategy
Tooling design	Content Uniformity	Low	Tooling design was selected to compress a tablet with a similar size and shape as the RLD. No picking was observed during the final blending and lubrication studies. The risk is low.
	Dissolution	Low	
Feed frame paddle speed	Content Uniformity	High	A greater than optimal feed frame paddle speed may cause over-lubrication. A lower than optimal feed frame paddle speed may cause inconsistent die filling. The risk is high.
	Dissolution	High	
Feeder fill depth	Content Uniformity	Low	The feeder fill depth is set to 80% full and is monitored and controlled by an automatic feedback control loop on the tablet press. The risk is low.
	Dissolution	Low	
Pre-compression force	Content Uniformity	Low	CU is dominated by BU and flowability and is unrelated to pre-compression force. The risk is low. A greater than optimal pre-compression force may cause lamination. A lower than optimal pre-compression force may trap air in the tablets, leading to capping. Either scenario could impact dissolution. The pre-compression force is set to 1.0 kN based on experience with similar formulations compressed on the same equipment. Adjustment may be needed. The risk is medium.
	Dissolution	Medium	
Main compression force	Content Uniformity	Low	CU is dominated by BU and flowability and is unrelated to main compression force. The risk is low. Suboptimal compression force may affect tablet hardness and friability and, ultimately, dissolution. The risk is high.
	Dissolution	High	
Press speed (dwell time)	Content Uniformity	High	A faster than optimal press speed may cause inconsistent die filling and weight variability which may then impact CU and dissolution. For efficiency, the press speed will be set as fast as practically possible without adversely impacting tablet quality. The risk is high.
	Dissolution	High	
Hopper design and vibration	Content Uniformity	Low	Since acetriptan is roller compacted with excipients, the risk of drug substance segregation is minimized. Tablet press vibrations and the hopper angle design are unlikely to have an impact on CU and dissolution. The risk is low.
	Dissolution	Low	
Hopper fill level	Content Uniformity	Low	The blend has acceptable flowability and the hopper fill level is maintained at 50%. Maintaining the hopper fill level makes it improbable that this parameter will impact CU and dissolution. The risk is low.
	Dissolution	Low	
Drop height of finished tablets	Content Uniformity	Medium	Finished tablets may chip, crack, cleave or break if the drop height is great. The risk is medium.
	Dissolution	Medium	
Compression run time	Content Uniformity	Medium	It is possible during long compression run times that the CU may drift. The risk is medium. It is unlikely for compression run time to cause a drift that leads to a dissolution failure. The risk is low.
	Dissolution	Low	

Process Step: Tablet Compression			
Drug Product CQAs: Content Uniformity, Dissolution			
Variables	Drug Product CQAs	Risk Assessment	Justification and Initial Strategy
Environment (temperature and RH)	Content Uniformity	Low	If not controlled, fluctuations in the facility temperature and RH could impact the CQAs. Routine environment temperature and RH set point in the cGMP manufacturing facility is fixed at 25 °C ± 5% and 40%-60% RH, respectively, and will be monitored during manufacturing. The risk is low.
	Dissolution	Low	

The following experiments were undertaken to investigate the relationship between the input material attributes (i.e., ribbon relative density) and process parameters related to compression and the final drug product quality attributes. Three batches of final blend (Batch No. 53-55, 15.0 kg each, drug substance Lot #2) were manufactured in a 50 L blender for the compression studies. The ribbon relative density for these three batches was 0.68, 0.75 and 0.81, respectively. The roller compaction studies concluded that within this range, the necessary compression force will not exceed the maximum allowable tool tip pressure recommended by the manufacturer.

Effect of Feeder Frame Paddle Speed

A screening study to investigate the impact of the feeder frame paddle speed (8-20 rpm) on tablet quality attributes was conducted. Since the final blend flows well, changes in feeder frame paddle speed within the specified range had no impact on tablet weight variability or content uniformity. Tablet dissolution was also unaffected by changes in feeder speed, suggesting that over-lubrication due to the additional mixing is not a concern. This process variable was eliminated from further study.

Effect of Main Compression Force, Press Speed and Ribbon Relative Density

Compression force and press speed (which is related to dwell time) can affect numerous quality attributes including hardness, disintegration, dissolution, assay, content uniformity, friability, weight variability and appearance. The density of the ribbon following roller compaction may also impact the compressibility and compactability of the granules which would then impact tablet hardness and dissolution. Therefore, a 2³ full factorial DOE with three center points was performed to understand the effects of these parameters on tablet quality attributes. Pre-compression force is important to reduce entrapped air that can impact the tablet integrity. However, based on previous experience with similar formulations compressed with similar tooling (ANDA 123456), the pre-compression force was fixed to 1 kN for this DOE. Table 46 presents the study design and acceptance criteria for the responses.

Table 46. Design of the 2³ full factorial DOE to investigate tablet compression

Factors: Process Parameters		Levels		
		-1	0	+1
A	Main compression force (kN)	5	10	15
B	Press speed (rpm)	20	40	60
C	Ribbon relative density (no units)	0.68	0.75	0.81
Responses		Goal		Acceptable Ranges
Y ₁	Appearance	Smooth, elegant appearance		
Y ₂	Hardness (kP)	Define acceptable range		To be defined based on other responses
Y ₃	Friability (%)	Minimize		NMT 1.0 %
Y ₄	Weight variability (%)	Minimize		Individual: Target ± 5% Composite: Target ± 3%
Y ₅	Assay (% w/w)	Achieve 100% w/w		95.0-105.0% w/w
Y ₆	Content uniformity (% RSD)	Minimize % RSD		% RSD < 5%
Y ₇	Disintegration time (min)	Minimize		NMT 5 min
Y ₈	Dissolution (%)	Maximize		NLT 80% at 30 min

The press was run at the speed of the specified DOE for at least five minutes prior to any sampling. Tablet samples were then pulled at the beginning, middle and end of each run (except for Batch No. 54c which was sampled every 20 min throughout the entire run). Similar responses were observed at each sample time point; therefore, Table 47 presents the results for the middle time point (*responses Y₁, Y₃, Y₄, Y₅ and Y₇ not shown*).

Table 47. Experimental results of the 2³ full factorial DOE to investigate tablet compression

Batch No.	Factors: Process Variables			Responses		
	A: Main compression force	B: Press speed	C: Ribbon relative density	Y ₂ : Hardness	Y ₆ : CU	Y ₈ : Dissolution at 30 min
	(kN)	(rpm)	--	(kP)	(% RSD)	(%)
55a	15	20	0.81	10.8	1.9	95.7
54a	10	40	0.75	9.7	3.1	96.1
53a	15	60	0.68	12.9	3.5	85.4
55b	15	60	0.81	11.3	3.9	92.6
53b	5	20	0.68	7.8	2.6	96.4
53c	15	20	0.68	13.6	2.2	83.8
55c	5	60	0.81	4.2	3.3	99.6
54b	10	40	0.75	10.4	2.9	94.5
55d	5	20	0.81	5.5	2.3	97.2
54c	10	40	0.75	9.1	2.5	93.1
53d	5	60	0.68	6.7	3.7	97.1

Significant factors for tablet hardness

Since center points were included in the study design, the significance of the curvature effect was tested using an adjusted model and was found to be not significant. Thus, center points were included for model fitting. As shown in the following half-normal plot (Figure 39), A (main compression force) was the dominating factor affecting tablet

hardness followed by C (ribbon relative density). The remaining model terms had no significant impact because they came from the normally distributed population as pure error based on Shapiro-Wilk hypothesis test results.

Hardness (kP)

Shapiro-Wilk Test

W-value = 0.868

p-value = 0.258

A: Main compression force (kN)

B: Press speed (rpm)

C: Ribbon relative density

▲ Error Estimates

■ Positive Effects

■ Negative Effects

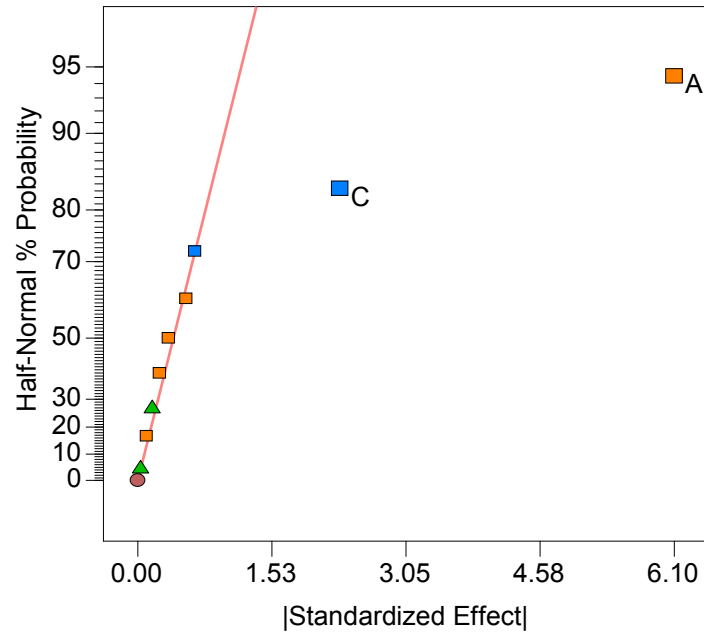


Figure 39. Half-normal plot of the compression variable effects on tablet hardness

Tablet hardness was directly related to main compression force and inversely related to ribbon relative density as shown in the contour plot below (Figure 40). Both the half-normal plot and the contour plot show that there was no interaction between these two factors.

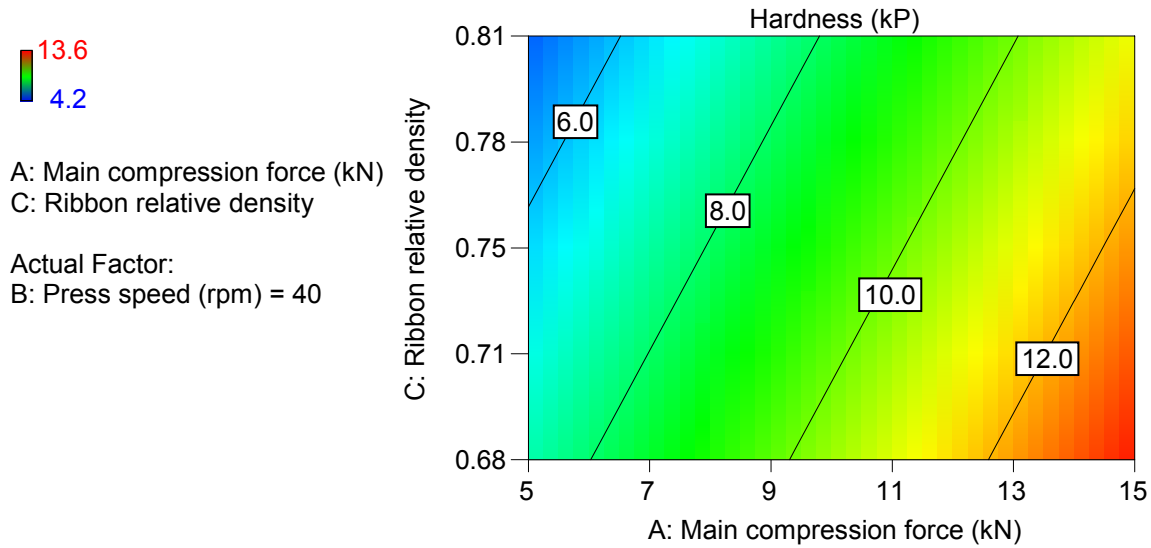


Figure 40. Effect of main compression force and ribbon relative density on tablet hardness

A roller compacted ribbon that exhibits a relative density toward the upper end of the acceptable range (0.81) required a greater compression force to achieve the same hardness than ribbon with a relative density toward the lower end of the acceptable range (0.68). This is because the powder mixture loses some of its compressibility and compactability after roller compaction.

The DOE results show that it is possible to adjust a process parameter to accommodate variability in a material attribute. In other words, the model can be used to determine the necessary compression force for a given ribbon relative density to ensure that the target tablet hardness is achieved.

Significant factors for tablet friability

None of the factors had a significant effect on tablet friability. All of the batches showed friability less than 0.2% except for Batch No. 55c which had an average hardness of 4.2 kP and showed a higher weight loss of 0.6%. Therefore, the lower limit for tablet hardness was set to 5.0 kP.

Significant factors for tablet weight variability and content uniformity

The half-normal plot below (Figure 41) shows that press speed was the only factor that had a significant impact on content uniformity. The effect was a positive effect, meaning that the % RSD increased as press speed increased. This is also shown clearly in the main effect plot (Figure 42). The main effect plot demonstrates that no curvature was observed so further optimization of the press speed is unnecessary.

Content Uniformity (% RSD)

Shapiro-Wilk Test
 W-value = 0.866
 p-value = 0.210

A: Main compression force (kN)
 B: Press speed (rpm)
 C: Ribbon relative density

▲ Error Estimates
 ■ Positive Effects
 ■ Negative Effects

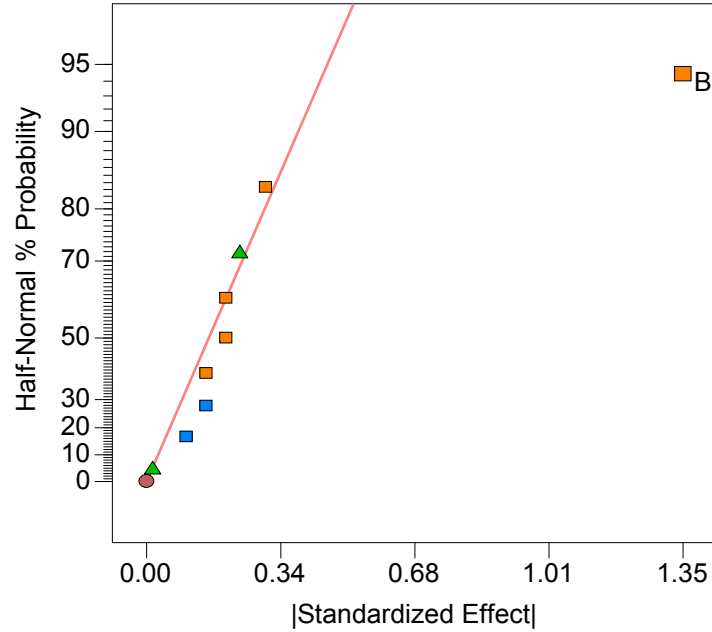


Figure 41. Half-normal plot of the compression variable effects on tablet content uniformity

Content Uniformity (% RSD)

B: Press speed (rpm)

Actual Factors:
 A: Main compression force (kN) = 10
 C: Ribbon relative density = 0.75

● Design Points

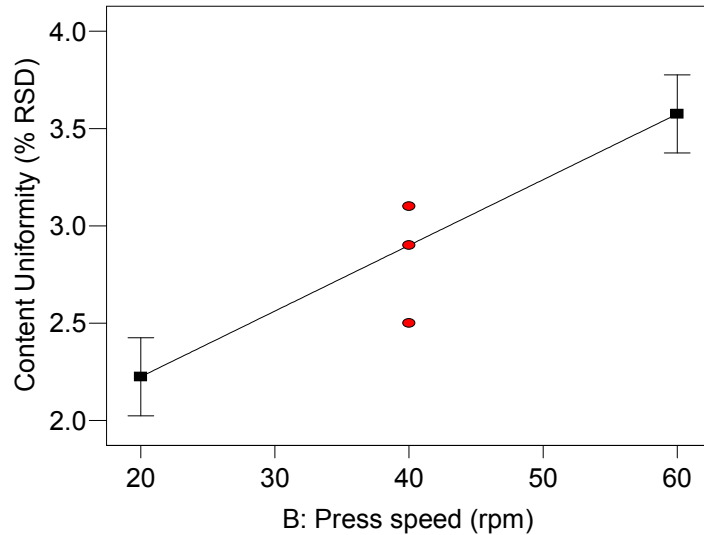


Figure 42. Main effect of press speed on tablet content uniformity

Although better content uniformity (i.e., lower % RSD) is achieved when the tablet press is operated at a slower speed, the press speed range investigated (20-60 rpm) did not result in out-of-specification tablet content uniformity. At 60 rpm, the % RSD observed was less than 4% and well below the limit of 5%.

Similarly, press speed had a statistically significant impact on tablet weight variability which increased with faster press speed. However, the individual tablet weight variability was well below 5% and the composite weight variability was well below 3%.

During production, it is desirable to maximize efficiency by setting the tablet press as fast as practically possible without adversely impacting the quality of the drug product. Based on the compression study, the proven acceptable range for press speed is 20-60 rpm.

Significant factors for tablet disintegration and dissolution

The main compression force, press speed, and ribbon relative density did not have a significant impact on disintegration. The disintegration time was rapid and varied from 1.5 minutes to 3 minutes.

The following half-normal plot (Figure 43) shows that the significant factors affecting the dissolution rate of the compressed tablets were A (main compression force) and C (ribbon relative density). These two factors also showed a significant interaction, AC. The remaining model terms had no significant impact based on Shapiro-Wilk hypothesis test results.

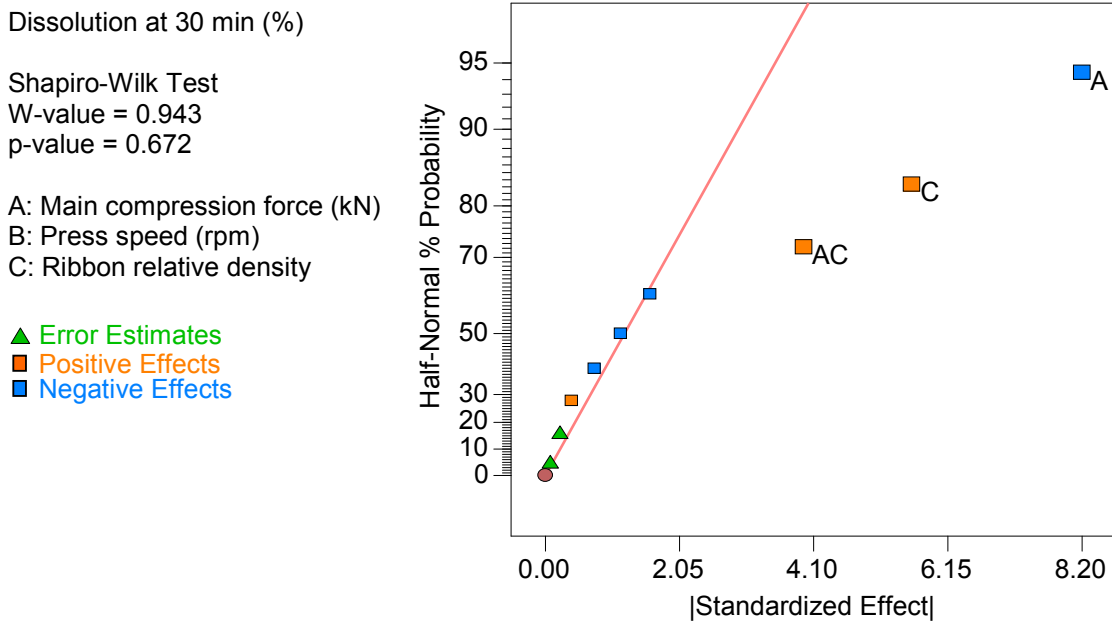


Figure 43. Half-normal plot of the compression variable effects on dissolution

Figure 44 illustrates the effect of main compression force and ribbon relative density on tablet dissolution. The curved contour lines show that an interaction exists because the dissolution results differed depending on the main compression force setting and the ribbon relative density. The dissolution rate decreased with increasing main compression force and increased with increasing ribbon relative density. These results are in line with the observed effect that these factors had on tablet hardness. Increasing the main compression force resulted in harder tablets and retarded dissolution even though rapid disintegration was still achieved by using 5% superdisintegrant. To avoid a potential dissolution failure, the upper limit for hardness is set to 13.0 kP since Batch No. 53c with a hardness of 13.6 kP showed dissolution of 83.8%.

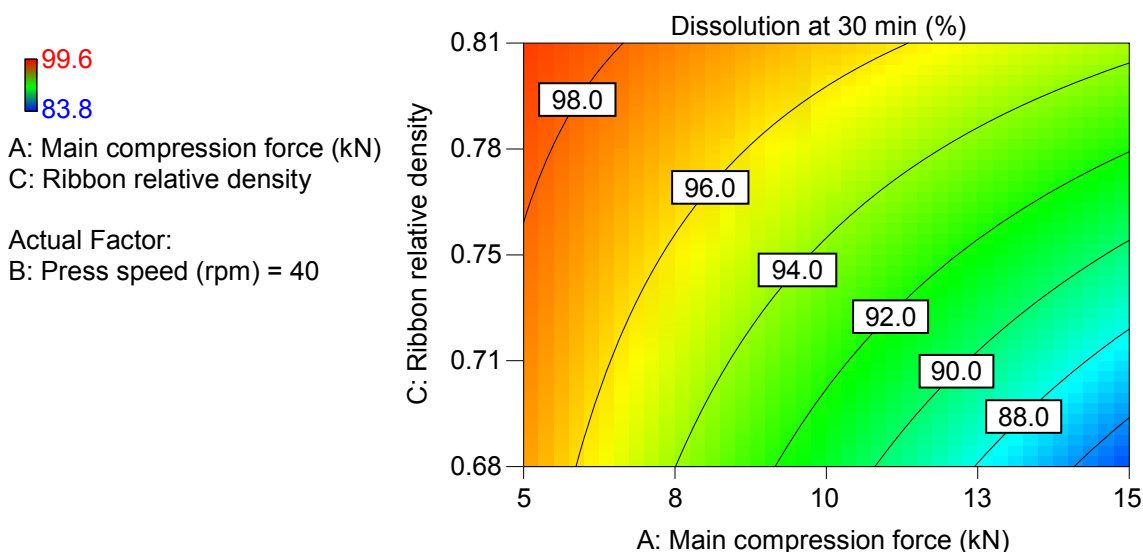


Figure 44. Effect of main compression force and ribbon relative density on tablet dissolution

Effect of compression run time on tablet weight variability

Batch No. 54c was sampled every 20 minutes to evaluate the potential drift in tablet weight over the course of the compression run. The results demonstrated that the weight variability was well controlled for the individual tablets within $\pm 5\%$ of the target weight and for the composite sample within $\pm 3\%$ of the target weight. No trend for tablet weight was observed throughout the entire compression run. Tablet samples pulled at the beginning, middle, and end of the run were tested for all DOE responses and results are shown in Table 47.

Summary of other responses

Main compression force, press speed, and relative ribbon density had no significant impact on the remaining responses. Each run produced tablets that had a smooth surface with no evidence of picking/sticking or capping. Assay ranged from 99.1% to 101.0%.

Summary of Tablet Compression Process Development

Within the range studied (8-20 rpm), feeder frame paddle speed did not impact the tablet dissolution. A press speed in the range of 20-60 rpm did not show any significant impact on the responses investigated. An acceptable range for compression force was identified. Force adjustments can be made to accommodate the acceptable variation in ribbon relative density (0.68-0.81) between batches.

Proposed Tablet Compression In-Process Controls

Based on the results of the studies undertaken to understand the process variables affecting compression, Table 48 lists the proposed in-process controls for the compression step.

Table 48. Proposed in-process controls for the compression step

Test	Frequency	Limits
Individual tablet weight (n = 10)	30 min	200.0 mg ± 10.0 mg
Composite tablet weight (n = 20)	30 min	4.00 g ± 0.12 g
Hardness (n = 10)	30 min	Target: 8.0-10.0 kP Limits: 5.0-13.0 kP
Thickness (n = 10)	30 min	3.00 mm ± 0.09 mm
Disintegration* (n = 6)	3× per run	NMT 5 min
Friability* (sample weight = 6.5 g)	3× per run	NMT 1.0%

*Tested at the beginning, middle and end of the run.

Updated Risk Assessment of the Tablet Compression Process Variables

The risks identified during the initial assessment of the compression step were reduced through development studies. The updated risk assessment is presented in Table 49.

Table 49. Updated risk assessment of the tablet compression process variables

Process Step: Tablet Compression			
Drug Product CQAs: Content Uniformity, Dissolution			
Variables	Drug Product CQAs	Risk Assessment	Justification for the Reduced Risks
Blend compressibility and compactability	Dissolution	Low	Compression force can be adjusted to accommodate the acceptable ribbon relative density (0.68-0.81) in order to achieve the target tablet hardness. The risk is reduced from high to low.
	Content Uniformity	Low	Feeder frame paddle speed in the range of 8-20 rpm had no impact on CU or dissolution. The same tablet press model will be used for pilot scale and commercial scale manufacture. If necessary, slight adjustments in the feeder frame paddle speed may be made when all stations are utilized. The risk is reduced from high to low.
Feeder frame paddle speed	Dissolution	Low	
Main compression force	Dissolution	Low	Tablet hardness increases with compression force. Within the compression force range studied, the resulting tablet hardness did not adversely affect dissolution and > 90% dissolution at 30 min was achieved. The risk is reduced from high to low.
Press speed (dwell time)	Content Uniformity	Low	A press speed of 20-60 rpm had no impact on CU or dissolution. Thus, the risk is reduced from high to low.
	Dissolution	Low	

2.3.6 Scale-Up from Lab to Pilot Scale and Commercial Scale

Note to Reader: Currently, scale-up information is limited at the time of submission. The applicant should discuss product specific scale-up principles including their planned approach to scale-up the process. OGD will evaluate the applicant's plan to determine

its adequacy. However, if a substantial amendment needs to be submitted due to the inadequacy of the scale-up plan, it may significantly extend the review process. It is the firm's discretion to submit scale-up data such as actual process verification information at the time of submission for a complex drug product which has a high risk of scale-up failure; however, in some cases it may be requested by OGD.

Process development was conducted on the lab scale (5.0 kg). This section describes the principles used to scale-up the process to the pilot scale (50.0 kg) in order to manufacture the exhibit batch. The same principles will be employed to scale-up the process to the commercial scale upon approval. Table 50 summarizes the different process scales.

Table 50. Process scale summary

Scale	Batch Size	Units
--	(kg)	--
Lab (Process Development)	5.0	25,000
Pilot (Exhibit)	50.0	250,000
Commercial (Proposed)	150.0	750,000

2.3.6.1 Scale-Up of the Pre-Roller Compaction Blending and Lubrication Process

The process development work for the pre-roller compaction blending and lubrication step was carried out in a 16 qt capacity twin shell V-blender. To scale-up, it was desirable to maintain geometric, dynamic and kinematic similarity by applying the following rules:

- *Geometric similarity*: keeping the ratio of all lengths constant (constant fill ratio)
- *Dynamic similarity*: maintaining constant forces (Froude number F_r)

$$F_r = \frac{rpm^2 R}{g}$$

rpm: revolutions per minute

R: characteristic radius

g: gravitational constant

- *Kinematic similarity*: maintaining a consistent number of revolutions (rpm × minutes)

At the pilot scale, the fill level was 74%. This was slightly higher than the fill level at lab scale which was 63%. The rotation speed at both scales was fixed due to equipment constraints. Although the target blending endpoint could be estimated by maintaining similarity between the scales, the final endpoint was determined using the validated in-line NIR method (*details provided in Section 3.2.P.5.3 Validation of Analytical Procedures*). To assess homogeneity of the blend, a moving block % RSD was calculated for each moving block of ten consecutive spectra and plotted as a function of time. The blend was considered uniform once the % RSD was below 5% for ten consecutive measurements.

The pre-roller compaction blending and lubrication process scale-up is summarized in Table 51.

Table 51. Scale up of pre-roller compaction blending and lubrication

Scale	Batch size		Blender capacity (L)	Volume fill level (%)	Rotation speed (rpm)	N _{rev} *	
	(kg)	(units)				Acetripitan PSD	N _{rev}
--							
Lab	5.0	25,000	17.6 (16 qt)	63	20	d ₉₀ = 10 μm	368
						d ₉₀ = 20 μm	285
						d ₉₀ = 30 μm	234
Pilot	50.0	250,000	150	74	12	285	
Commercial (Proposed)	150.0	750,000	500	67	8	To be determined	

*Endpoint determined by a validated in-line NIR method

2.3.6.2 Scale-Up of the Roller Compaction and Integrated Milling Process

For this drug product, the roller compaction process first needed to be scaled up from lab scale (using Alexanderwerk WP120 with 120 mm roll diameter and 25 mm roll width) to pilot scale (using Alexanderwerk WP120 with 120 mm roll diameter and 40 mm roll width) and then, ultimately, to commercial scale (using Alexanderwerk WP200 with 200 mm roll diameter and 75 mm roll width).

In a roller compaction process, there are several process parameters to consider when scaling up to a larger, wider roller. The strategy employed for each process parameter is discussed below.

Roller Gap

The scale-up strategy for the roller gap was to maintain the ratio between the roller gap (S) and the roller diameter (D) for different size roller compactors. The scale-up factor for the roller gap was calculated according to the following equation:

$$\frac{S1}{D1} = \frac{S2}{D2}$$

Roll Force or Roll Pressure

Based on the process development work, ribbon density was an intermediate critical quality attribute for this process step and strongly affected the downstream compression force required to meet the target tablet hardness. A commonly used strategy to scale-up roller compaction is to control the ribbon density by maintaining the roller peak pressure (P_{max}) as described by Johanson's model.¹³

According to the model, if the S/D ratio is maintained, a scale-up strategy is to obtain the same P_{max} by maintaining the $R_f/(W \times D)$ ratio where R_f is the roller force and W is the roller width. The scale-up factor for roller force is calculated by:

$$\frac{R_{f2}}{R_{f1}} = \frac{W_2 D_2}{W_1 D_1}$$

If roller hydraulic pressure is used, it is necessary to obtain the conversion factor between roller hydraulic pressure (bar) to roller force (kN) from the equipment vendor.

Alexanderwerk provided the following information:

For WP120: 0.0922 kN per cm of roller width for 1 bar roller pressure

For WP200: 0.0869 kN per cm of roller width for 1 bar roller pressure

The scale-up factor for roller pressure was calculated by:

$$\frac{R_{p2}}{R_{p1}} = \frac{0.0869 \times D_2}{0.0922 \times D_1}$$

Screw Speed and Roll Speed

Assuming no slip at the roller surface in the nip region (i.e., the material is moving at the same speed as the rollers), the mass flow rate (throughput, Q , g/min) of material can be calculated based on mass balance:

$$Q = \rho \pi D W S N_R$$

where ρ is the ribbon density (g/cc), D is the roller diameter (cm), W is the roller width (cm), S is the roller gap (cm) and N_R is the roller rotation speed (rpm).

The powder material is conveyed to the rollers by the screw auger and the mass flow rate is typically proportional to the screw rotation rate:

$$Q = C_S N_S$$

where, N_S is the feed screw rotation speed (rpm) and C_S is the amount of material conveyed by the screw per rotation (g/rotation) which can be determined experimentally. To achieve the target ribbon density for the given roller gap, the ratio of screw speed to roller speed was maintained constant by setting the two equations for mass flow rate equal to each other as shown below:

$$\frac{N_S}{N_R} = \frac{\rho \pi D W S}{C_S}$$

Mill Screen Orifice Size and Mill Speed

Mill screen orifice size is a scale-independent variable; therefore, it is kept constant upon scale-up. During development, mill speed was not found to be critical for any product

quality attributes. In practice, mill speed is set based on first-in first-out principles to avoid ribbon accumulation in the mill.

Table 52 summarizes the roller compaction and integrated milling process scale-up.

Table 52. Scale-up of the roller compaction and integrated milling process

Scale	Batch Size		Alexanderwerk model	Roller width (mm)	Roller diameter (mm)	Roller gap (mm)	Roller pressure (bar)	Mill screen orifice size (mm)
	(kg)	(units)						
--			--					
Lab	5.0	25,000	WP120	25	120	1.2-2.4	20-77	1.0
Pilot	50.0	250,000	WP120	40	120	1.8	50	1.0
Commercial (Proposed)	150.0	750,000	WP200	75	200	2.0-4.0*	31-121*	1.0

*The range is based on the scale-up equation and needs to be verified.

2.3.6.3 Scale-Up of the Final Blending and Lubrication Process

To scale-up the final blending of the granules with talc, the number of revolutions was maintained.

A different strategy was employed to scale-up the final lubrication. Recently, an equation for scaling up the lubrication of a 1:1 MCC:Lactose blend with magnesium stearate was published.¹⁶ If the batch size and blender volume of the new process are known, the number of revolutions to be used at the new process condition can be evaluated using the following equation:

$$r_2 = \frac{(V^{1/3} F_{headspace} r)_1}{(V^{1/3} F_{headspace})_2}$$

where V is the blender volume, $F_{headspace}$ is the headspace fraction (calculated by 100% - fill level %), and r is the number of revolutions. The number of revolutions needed to lubricate the granules with magnesium stearate was calculated based on this equation. The final blending and lubrication process scale-up is summarized in Table 53.

¹⁶ Kushner IV, J., Moore, F., 2010. Scale-up model describing the impact of lubrication on tablet tensile strength. International Journal of Pharmaceutics. 399, 19-30.

Table 53. Scale-up of the final blending and lubrication

Scale	Batch size		Blender capacity (L)	Volume fill level (%)	Rotation speed (rpm)	Final Blending		Lubrication	
	(kg)	(units)				(min)	--	(min)	--
Lab	5.0	25,000	17.6 (16 qt)	49	20	5	100	3-5	60-100
Pilot	50.0	250,000	150	56	12	8.3	100	4	48
Commercial (Proposed)	150.0	750,000	500	50	8	12.5*	100*	~2.6-4.3*	21-35*

*To be verified

2.3.6.4 Scale-Up of the Tablet Compression Process

The same tablet press utilized during the tablet compression process development studies was used for the pilot batch and will be used for commercial scale production. Detailed parameters that affect the tableting process were already explored and discussed in *Section 2.3.5*. To increase throughput, all 51 stations were used at the pilot scale successfully and will be used at the commercial scale. The press will be run at the same speed that was studied during development (20-60 rpm). Therefore, dwell time remains unchanged during scale-up.

2.3.7 Exhibit Batch

Based on the scale-up principles detailed in *Section 2.3.6*, a 50.0 kg cGMP exhibit batch was manufactured with drug substance Lot #2 at the pilot scale and the batch was used for the pivotal BE study. Table 54 summarizes the equipment and process parameters used for the exhibit batch at pilot scale.

Table 54. Equipment and process parameters used for the exhibit batch at pilot scale

Process Steps	Equipment and Process Parameters
Pre-Roller Compaction Blending and Lubrication	150 L V-blender <ul style="list-style-type: none"> ○ 285 revolutions (target) for blending at 12 rpm (endpoint determined by an in-line NIR method)
Roller Compaction and Integrated Milling	Alexanderwerk WP120 with 40 mm roller width and 120 mm roller diameter <ul style="list-style-type: none"> ○ Roller surface: Knurled ○ Roller pressure: 50 bar ○ Roller gap: 1.8 mm ○ Roller speed: 8 rpm ○ Mill speed: 60 rpm ○ Coarse screen orifice size: 2.0 mm ○ Mill screen orifice size: 1.0 mm
Final Blending and Lubrication	150 L V-blender <ul style="list-style-type: none"> ○ 100 revolutions for granule and talc blending (8.3 min at 12 rpm) ○ 48 revolutions for lubrication (4 min at 12 rpm)
Tablet Compression	51 station rotary press (51 stations used) <ul style="list-style-type: none"> ○ 8 mm standard round concave tools ○ Press speed: 40 rpm ○ Compression force: 8-11 kN <ul style="list-style-type: none"> • Target hardness 8.0-10.0 kP ○ Pre-compression force: 1.0 kN

The in-process testing and final release results are summarized in Table 55 and Table 56, respectively.

Table 55. In-process testing results for the exhibit batch (Batch No. DPJM032012)

Test	In-Process Controls	Results
Pre-Roller Compaction Blending and Lubrication		
Blend Uniformity	NIR % RSD < 5%	4.9%
Roller Compaction and Integrated Milling		
Ribbon relative density	0.68-0.81	0.74
Granule PSD	d ₁₀	50-150 µm
	d ₅₀	400-800 µm
	d ₉₀	800-1200 µm
Granule Uniformity	% RSD < 5%	4.3%
Flow function coefficient (ffc)	> 6	7.35
Final Blending and Lubrication		
Blend Uniformity	% RSD < 5%	2.7%
Blend Assay	95.0-105.0% w/w	100.2% w/w
Tablet Compression		
Individual tablet weight (n = 10)	200.0 mg ± 10.0 mg	197.2-202.8 mg
Composite tablet weight (n = 20)	4.00 g ± 0.12 g	4.04 g
Hardness (n = 10)	Target: 8.0-10.0 kP Limits: 5.0-13.0 kP	8.8-9.3 kP
Thickness (n = 10)	3.00 mm ± 0.09 mm	2.97-3.03 mm
Disintegration (n = 6)	NMT 5 min	1.5 min
Friability (sample weight = 6.5 g)	NMT 1.0 % w/w	0.1% w/w

Table 56. Release testing results for the exhibit batch (Batch No. DPJM032012)

Test	Acceptance Criteria	Results
Description	White to off-white, round convex tablet embossed with GEN-ACE and 20	White to off-white, round convex tablet embossed with GEN-ACE and 20
Identification	A. HPLC Retention time: corresponds to standard B. UV absorption: spectrum corresponds to standard	A. Corresponds to standard B. Corresponds to standard
Assay	95.0-105.0% w/w of label claim	100.3% w/w
Content Uniformity	AV < 15	AV = 4.7
Dissolution	NLT 80% in 30 minutes (in 900 mL of 0.1 N HCl with 1.0% w/v SLS using USP Apparatus 2 at 75 rpm)	96%
Degradation Products	ACE12345: NMT 0.5%, Individual unknown impurity: NMT 0.2%, Total impurities: NMT 1.0%	ACE12345: 0.1% Individual unknown impurity: 0.06% Total impurities: 0.22%
Residual Solvents	Complies with USP <467> Option I	Complies with USP <467> Option I

2.3.8 Updated Risk Assessment of the Drug Product Manufacturing Process

During process development, the identified high risks for each process step were addressed. Experimental studies were defined and executed in order to establish additional scientific knowledge and understanding, to allow appropriate controls to be developed and implemented, and to reduce the risk to an acceptable level. After detailed experimentation, the initial manufacturing process risk assessment was updated in line

with the current process understanding. Table 57 presents how the application of the control strategy to the manufacturing process has reduced the identified risks. Table 58 provides the justification for the reduced risk following process development.

Table 57. Updated risk assessment of the manufacturing process for Generic Acetripitan Tablets, 20 mg

Drug Product CQAs	Process Steps				
	Pre-RC Blending and Lubrication	Roller Compaction	Milling	Final Blending and Lubrication	Compression
Assay	Low	Low*	Low	Low*	Low
Content Uniformity	Low	Low	Low	Low*	Low
Dissolution	Low	Low	Low	Low	Low
Degradation Products	Low*	Low*	Low*	Low*	Low*

*The level of risk was not reduced from the initial risk assessment.

Table 58. Justification for the updated risk assessment of the manufacturing process for Generic Acetripitan Tablets, 20 mg

Process Steps	Drug Product CQAs	Justification for the Reduced Risks
Pre-Roller Compaction Blending and Lubrication	Assay	An in-line NIR method was developed and validated to determine the blending endpoint. Using the finalized formulation, all development batches and the exhibit batch achieved acceptable assay, CU and dissolution. The risk is reduced from high to low for CU and from medium to low for assay and dissolution.
	Content Uniformity	
	Dissolution	
Roller Compaction	Content Uniformity	Within a ribbon relative density range of 0.68-0.81, the resulting PSD of the milled granules had good flowability as measured by ffc. The risk is reduced from high to low.
	Dissolution	Within a ribbon relative density range of 0.68-0.81, the desired tablet hardness (8.0-10.0 kP) can be achieved by adjusting the compression force. The risk of roller compaction to impact dissolution is reduced from high to low.
Milling	Assay	The mill speed did not show a significant impact on any drug product quality attributes. The mill screen orifice size was found critical and set to 1.0 mm. With this selection, all CQAs can be achieved by using the appropriate range for roller pressure and roller gap. The risk of milling to impact assay, CU and dissolution is reduced to low.
	Content Uniformity	
	Dissolution	
Final Blending and Lubrication	Dissolution	Within the range studied, number of revolutions and magnesium stearate specific surface area did not exhibit a significant impact on disintegration or dissolution of the tablets. The risk is reduced from high to low.

Process Steps	Drug Product CQAs	Justification for the Reduced Risks
Compression	Assay	The development studies demonstrated that feed frame paddle speed and press speed did not significantly impact the tablet weight variability, assay or CU. The risk is reduced from high to low for CU and from medium to low for assay.
	Content Uniformity	
	Dissolution	Within a ribbon relative density range of 0.68-0.81, the desired tablet hardness (8.0-10.0 kP) can be achieved by adjusting the compression force. No over-lubrication of the blend was observed when the feed frame paddle speed was operated within the range studied (8-20 rpm). The risk is reduced from high to low.

2.4 Container Closure System

To be consistent with the RLD, the proposed generic drug product is intended to be labeled for storage at 25 °C (77 °F) with excursions permitted to 15-30 °C (59-86 °F). The innovator has chosen round white opaque HDPE bottles with an induction seal liner and child resistant (CR) closure. Generic Acetripitan Tablets, 20 mg, will be similarly packaged and the bottle pack details are summarized in Table 59.

Table 59. Proposed commercial packaging for Generic Acetripitan Tablets, 20 mg

Count	HDPE Bottle	Closure
30 Tablets	40 cc	33 mm white CR cap with pulp liner
90 Tablets	60 cc	38 mm white CR cap with pulp liner

2.5 Microbiological Attributes

An accelerated stability study of the exhibit batch demonstrated that the drug product has low water activity and is not capable of supporting microbial growth. Routine microbiological testing of Generic Acetripitan Tablets, 20 mg, is unnecessary due to the low water activity of the product and controls on incoming raw materials.

2.6 Compatibility

This section is not applicable because the drug product is a solid oral dosage form and there are no reconstitution diluents.

2.7 Control Strategy

Note to Reader: The control strategy is “a planned set of controls, derived from current product and process understanding, that assures process performance and product quality. The controls can include parameters and attributes related to drug substance and drug product materials and components, facility and equipment operating conditions, in-process controls, finished product specifications, and the associated methods and frequency of monitoring and control.”¹⁷

The control strategy for Generic Acetripitan Tablets, 20 mg, is built upon the outcome of extensive product and process understanding studies. These studies investigated the material attributes and process parameters that were deemed high risk to the CQAs of the drug product during the initial risk assessment. In some cases, variables considered medium risk were also investigated. Through these systematic studies, the CMAs and CPPs were identified and the acceptable operating ranges were established. All variables ranked as high risk in the initial risk assessment are included in the control strategy because the conclusion of the experiments was dependant on the range(s) studied and the complex multivariate relationship between variables. Thus, the control strategy is an integrated overview of how quality is assured based on current process and product knowledge. The control strategy may be further refined based on additional experience gained during the commercial lifecycle of the product. However, any post-approval changes should be reported to the agency in accordance with CFR 314.70 and should follow steps as outlined by guidances used for scale-up and post-approval changes.

The control strategy for the commercial manufacture of Generic Acetripitan Tablets, 20 mg, is proposed and presented in Table 60. The control strategy includes acetripitan and excipient material attributes to be controlled, in-process controls, high risk process parameter ranges studied during development and the proposed operating ranges for commercial manufacture. The purpose of the controls is also briefly discussed. The release specification for the final product is provided in Table 61.

¹⁷ ICH Harmonised Tripartite Guideline: Q10 Pharmaceutical Quality Systems. June 2008.

Table 60. Control Strategy for Generic Acetriptan Tablets, 20 mg

Factor	Attributes or Parameters	Range studied (lab scale)	Actual data for the exhibit batch (pilot scale)	Proposed range for commercial scale ¹	Purpose of control
Raw Material Attributes					
Acetriptan polymorphic form*	Melting point	185-187 °C	186 °C	185-187 °C	To ensure polymorphic Form III
	XRPD 2θ values	2θ: 7.9°, 12.4°, 19.1°, 25.2°	2θ: 7.9°, 12.4°, 19.1°, 25.2°	2θ: 7.9°, 12.4°, 19.1°, 25.2°	
Acetriptan particle size distribution*	d ₉₀	10-45 μm	20 μm	10-30 μm	To ensure in vitro dissolution, in vivo performance and batch-to-batch consistency
	d ₅₀	6-39 μm	12 μm	6-24 μm	
	d ₁₀	3.6-33.4 μm	7.2 μm	3.6-14.4 μm	
Lactose Monohydrate, Grade A01	Particle size distribution	d ₅₀ : 70-100 μm	d ₅₀ : 85 μm	d ₅₀ : 70-10 μm	To ensure sufficient flowability and batch-to-batch consistency
Microcrystalline Cellulose (MCC), Grade B02	Particle size distribution	d ₅₀ : 80-140 μm	d ₅₀ : 108 μm	d ₅₀ : 80-140 μm	
Croscarmellose Sodium (CCS), Grade C03	Particle size distribution	> 75 μm: NMT 2%	> 75 μm: 1%	> 75 μm: NMT 2%	To ensure batch-to-batch consistency
		> 45 μm: NMT 10%	> 45 μm: 4%	> 45 μm: NMT 10%	
Talc, Grade D04	Particle size distribution	> 75μm: NMT 0.2%	> 75μm: 0.1%	>75μm: NMT 0.2%	To ensure batch-to-batch consistency
Magnesium Stearate, Grade E05	Specific surface area	5.8-10.4 m ² /g	8.2 m ² /g	5.8-10.4 m ² /g	To ensure sufficient lubrication and to reduce the risk of retarded disintegration and dissolution
Pre-Roller Compaction Blending and Lubrication Process Parameters					
V-blender	Number of revolutions*	250 (25 rpm, 10 min) 100-500 (20 rpm, 5-25 min)	285 revolutions (12 rpm, 23.8 min)	Target to be determined based on DS PSD	In-line NIR method is used for endpoint determination to ensure BU is met consistently
	Blender fill level	~50% (1.0 kg, 4 qt) 35-75% (5.0 kg, 16 qt)	~74% (50.0 kg, 150 L)	~67% (150.0 kg, 500 L)	

Example QbD IR Tablet Module 3 Quality 3.2.P.2 Pharmaceutical Development

Factor	Attributes or Parameters	Range studied (lab scale)	Actual data for the exhibit batch (pilot scale)	Proposed range for commercial scale ¹	Purpose of control
Pre-Roller Compaction Blending and Lubrication In-Process Controls					
Blend uniformity*	Blend to endpoint: < 5.0% RSD (In-line NIR method)				
Roller Compaction and Integrated Milling Process Parameters					
Roller compactor and integrated mill	Equipment	Alexanderwerk WP120 (roller diameter: 120 mm; roller width: 25 mm)	Alexanderwerk WP120 (roller diameter: 120 mm; roller width: 40 mm)	Alexanderwerk WP200 (roller diameter: 200 mm; roller width: 75 mm)	Fixed due to equipment availability
	Roller pressure*	20-80 bar	50 bar	31-121 bar	To ensure desired ribbon density, granule PSD, uniformity and flowability are achieved consistently
	Roller gap*	1.2-2.4 mm	1.8 mm	1.2-2.4 mm	
	Mill speed	20-100 rpm	60 rpm	20-100 rpm	
	Mill screen orifice size*	0.6-1.4 mm	1.0 mm	1.0 mm	
Roller Compaction and Integrated Milling Process In-Process Controls					
Ribbon relative density*	0.68-0.81				
Granule particle size distribution d ₁₀ *	50-150 μm				
Granule particle size distribution d ₅₀ *	400-800 μm				
Granule particle size distribution d ₉₀ *	800-1200 μm				
Granule uniformity*	% RSD < 5%				
Granule flowability (ffc)*	> 6.00				
Final Blending and Lubrication Process Parameters					
V-blender Final Blending (granules w/ talc)	Number of revolutions	100 (25 rpm, 4 min) 100 (20 rpm, 5min)	100 revolutions (12 rpm, 8.3 min)	100 revolutions (8 rpm, 12.5 min)	To ensure consistent mixing of granules and talc
	Blender fill level	~38% (1.0 kg, 4 qt) ~49% (5.0 kg, 16 qt)	~56% (50.0 kg, 150 L)	~50% (150.0 kg, 500 L)	
V-blender Lubrication (magnesium stearate)	Number of revolutions	75 (25 rpm, 3 min) 60-100 (20 rpm, 3-5 min)	48 revolutions (12 rpm, 4 min)	21-35 revolutions (8 rpm, 2.6-4.3 min)	To ensure lubricant is well distributed and to avoid over-lubrication
	Blender fill level	~38% (1.0 kg, 4 qt) ~49% (5.0 kg, 16 qt)	~56% (50.0 kg, 150 L)	~50% (150.0 kg, 500 L)	

Example QbD IR Tablet Module 3 Quality 3.2.P.2 Pharmaceutical Development

Factor	Attributes or Parameters	Range studied (lab scale)	Actual data for the exhibit batch (pilot scale)	Proposed range for commercial scale ¹	Purpose of control
Final Blending and Lubrication Process In-Process Controls					
Blend uniformity*		% RSD < 5%			
Blend assay*		95.0-105.0% w/w			
Tablet Compression Process Parameters					
Rotary press	Feeder frame paddle speed	8-20 rpm	15 rpm	8-20 rpm	To ensure all tablet CQAs (assay, CU and drug release) are met consistently
	Press speed	20-60 rpm	40 rpm	20-60 rpm	
	Pre-compression force	1.0 kN	1.0 kN	1.0 kN	
	Compression force*	5-15 kN	8-11 kN	To be determined based on ribbon relative density	
Tablet Compression In-Process Controls					
Individual weight (n = 10; every 20 min)		200.0 mg ± 10.0 mg			
Composite weight (n = 20; every 20 min)		4.00 g ± 0.12 g			
Hardness (n = 10; every 20 min)		Target: 8.0-10.0 kP, Limits: 5.0-13.0 kP			
Thickness (n = 10; every 20 min)		3.00 mm ± 0.09 mm			
Disintegration (n = 6; 3× during run)		NMT 5 min			
Friability (sample weight = 6.5 g; 3× during run)		NMT 1.0 %			

*critical input material attributes (CMA), critical process parameters (CPP) or critical quality attributes (CQA) of in-process material or final drug product

¹The proposed operating range for commercial scale will be qualified and continually verified.

Table 61. Generic Acetripitan Tablets, 20 mg release specification

Test	Acceptance Criteria
Description	White to off-white, round convex tablet embossed with GEN-ACE and 20
Identification	A. HPLC Retention time: corresponds to standard B. UV absorption: spectrum corresponds to standard
Assay	95.0-105.0% w/w of label claim
Content Uniformity	AV < 15
Dissolution	NLT 80% in 30 minutes (in 900 mL of 0.1 N HCl with 1.0% w/v SLS using USP Apparatus 2 at 75 rpm)
Degradation Products	ACE12345: NMT 0.5%, Individual unknown impurity: NMT 0.2%, Total impurities: NMT 1.0%
Residual Solvents	Complies with USP <467> Option I

2.7.1 Control Strategy for Raw Material Attributes

The drug substance particle size distribution limits arise from a combination of its impact on blending and in vivo performance. The pilot PK study suggested that Generic Acetripitan Tablets, 20 mg, with a drug substance d_{90} of 30 μm (d_{50} of 24 μm) or less would be bioequivalent to the RLD. During formulation development, a particle size distribution with a d_{90} value greater than 14 μm was found to ensure good flow and content uniformity using a fixed blending process. However, implementing a validated in-line NIR method to determine the blending endpoint during process development allowed acceptable blending uniformity and tablet CQAs to be achieved using a drug substance d_{90} in the range of 10-30 μm .

Excipient particle size distribution specifications were based on the attributes of the selected grades. For lactose and microcrystalline cellulose, an in-house limit is set on d_{50} to ensure batch-to-batch consistency.

Based on the analysis of dissolution data collected during formulation development and the results of the pilot PK study, the dissolution medium with 1.0% w/v SLS was more sensitive to product differences than the FDA-recommended method using medium with 2.0% w/v SLS. For this reason, 1.0% w/v SLS is used in the dissolution medium for the release method in the control strategy.

2.7.2 Control Strategy for Pre-Roller Compaction Blending and Lubrication

The updated risk assessment (Table 37) for the pre-roller compaction blending and lubrication process step demonstrates that the identified risks to blend uniformity have been reduced by adjusting the number of revolutions to accommodate different acetripitan particle size distributions. A validated in-line NIR method for monitoring the blend uniformity was developed, validated and implemented to terminate the blending based on

feedback control when the moving block % RSD of ten consecutive spectra is below 5% for ten consecutive measurements.

2.7.3 Control Strategy for Roller Compaction and Integrated Milling

The intent of the control strategy for roller compaction is to maintain the ribbon density within the required range to ensure drug product CQAs are met. To maintain a ribbon relative density of 0.68-0.81 during routine operation, the roller pressure and roller gap will be controlled. The ribbon density will be monitored as an in-process control during roller compaction.

For milling, the mill screen orifice size (1.0 mm) was selected to ensure that the granule size distribution remains within the acceptable range. The acceptable range for mill speed (20-100 rpm) was established and can be adjusted within the range to accommodate different throughput from the roller compaction step. If a change to the mill screen orifice size is made (e.g., increase or decrease) then the impact on granule size distribution and assay of sieve cuts will be reassessed across the pre-defined ribbon density range.

2.7.4 Control Strategy for Final Blending and Lubrication

The control strategy for blending the granules with talc is to maintain the targeted number of revolutions. For the granule lubrication with magnesium stearate, the control strategy is to adjust the number of revolutions based on the blender capacity used (headspace) and the volume of the V-blender according to the scientific literature.

2.7.5 Control Strategy for Tablet Compression

The control strategy for compression is to maintain the in-process tablet attributes of weight, hardness, thickness, friability and disintegration within the required ranges. The fill cam below the die table adjusts the lower punch to the appropriate height to control fill depth and ultimately tablet weight. The target compression force required to produce tablets with the desired hardness, and ultimately friability and disintegration, is established at the beginning of each run. After tablets with the target weight and hardness are obtained during the tablet press set-up, the upper punch penetration depth and the fill depth are fixed. The compression force is continuously measured throughout the run for each tablet and compared to the target compression force. The main compression height is automatically adjusted to keep the average force as close as possible to the target set point. Upper and lower limits of compression force are set and any tablet that registers a compression force outside these limits is automatically rejected by the tablet press.

2.7.6 Product Lifecycle Management and Continual Improvement

Upon approval, the manufacturing process for Generic Acetripitan Tablets, 20 mg, will be validated using the lifecycle approach that employs risk-based decision making throughout the drug product lifecycle as defined in the FDA process validation guidance.¹⁸

The QbD approach taken during pharmaceutical development of Generic Acetripitan Tablets, 20 mg, facilitated product and process understanding relevant to Stage 1 (Process Design) of process validation. During Stage 1, the commercial manufacturing process was defined based on knowledge gained through development and scale up activities and a strategy for process control was developed. The goal of Stage 2 (Process Qualification) is to evaluate if the process is capable of reproducible commercial manufacturing. The manufacturing facility will be designed according to cGMP regulations on Building and Facilities.¹⁹ Activities will be taken to demonstrate that utilities and equipment are suitable for their intended use and perform properly. The protocol for process performance qualification will be written, reviewed, approved, and then executed to demonstrate that the commercial manufacturing process performs as expected. The goal of Stage 3 (Continued Process Verification) is continual assurance that the process remains in a state of control (the validated state) during commercial manufacture.

Throughout the product lifecycle, the manufacturing process performance will be monitored to ensure that it is working as anticipated to deliver the product with desired quality attributes. Process stability and process capability will be measured and evaluated. If any unexpected process variability is detected, appropriate actions will be taken to correct, anticipate, and prevent future problems so that the process remains in control. The additional knowledge gained during routine manufacturing will be utilized for adjustment of process parameters as part of the continual improvement of the drug product. As a commitment, the regulatory agency will be notified in accordance with CFR 314.70 regarding each change in each condition beyond the variability already provided in this application.

¹⁸ U.S. Food and Drug Administration. Guidance for Industry. Process Validation: General Principles and Practices. January 2011.

¹⁹ 21 CFR Part 211 Current Good Manufacturing Practice for Finished Pharmaceuticals, Subpart C.

List of Abbreviations

ANDA:	Abbreviated New Drug Application
ANOVA:	Analysis of Variance
AUC:	Area under the Curve
AV:	Acceptance Value
BE:	Bioequivalence
BU:	Blending Uniformity
CCS:	Croscarmellose Sodium
CFR:	Code of Federal Regulations
CMA:	Critical Material Attribute
C_{max} :	Maximum Plasma Concentration
CPP:	Critical Process Parameter
CQA:	Critical Quality Attribute
CU:	Content Uniformity
df:	degrees of freedom
DOE:	Design of Experiments
DS:	Drug Substance
DSC:	Differential Scanning Calorimetry
ffc:	flow function coefficient
ICH:	International Conference on Harmonization
IR:	Immediate Release
LOD:	Loss on Drying
MCC:	Microcrystalline Cellulose
N/A:	Not applicable
ND:	Not detected
NIR:	Near-infrared
NLT:	Not Less Than
NMT:	Not More Than
No.:	Number
N_{rev} :	Number of revolutions
PK:	Pharmacokinetic
PSD:	Particle Size Distribution
QbD:	Quality by Design
QTPP:	Quality Target Product Profile
R^2 :	Coefficient of Determination
RC:	Roller Compaction
RLD:	Reference Listed Drug (Product)
RSD:	Relative Standard Deviation
RT:	Room Temperature
SLS:	Sodium Lauryl Sulfate
TI:	Tolerance interval
T_{max} :	Time for achieving Maximum Plasma Concentration
XRPD:	X-Ray Powder Diffraction